

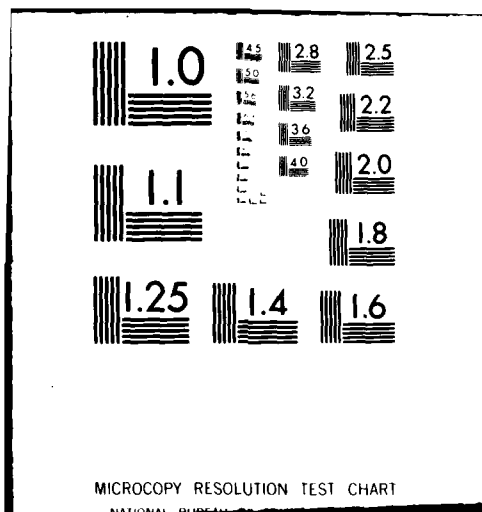
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A NUMERICAL TECHNIQUE FOR THE  
CALCULATION OF DISPERSION RELATIONS  
AND MODE FUNCTIONS FOR UPPER  
OCEAN INTERNAL WAVES

Irvin W. Kay  
Patricia J. Draper  
Wasył Wasyłkiwskyj

October 1980

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the dispersion relation, which is obtained numerically by solving the equation by means of the method of *regula falsi*. A computer program that performs the necessary calculations is described and listed.

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**A NUMERICAL TECHNIQUE FOR THE  
CALCULATION OF DISPERSION RELATIONS  
AND MODE FUNCTIONS FOR UPPER  
OCEAN INTERNAL WAVES**

**Irvin W. Kay  
Patricia J. Draper  
Wasył Wasyłkiwskyj**

**October 1980**

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## CONTENTS

I.	INTRODUCTION	1
II.	DESCRIPTION OF THE PROBLEM AND SOME GENERAL PROPERTIES OF INTEREST	5
III.	THE NUMERICAL PROCEDURE TO DETERMINE DISPERSION RELATIONS	9
IV.	DETAILS OF THE NUMERICAL PROCEDURE	15
	A. SOLUTION OF THE DIFFERENTIAL EQUATION	15
	B. SOLUTION OF THE EIGENVALUE EQUATION	16
	C. SELECTING INCREMENTS OF $\mu$	16
	D. ESTIMATING THE ERROR IN K	17
V.	COMPUTER REALIZATION OF THE ALGORITHM	19
	A. INPUTS	19
	1. NAMELIST/PARAM/XO, B, STOPK, STOPMU, ND, EPS	19
	2. Data Cards	20
	B. OUTPUTS	20
	1. Printout	20
	2. Disk or Tape	20
	3. Plot	21
	C. EXTERNAL REFERENCES	21
	1. INTMODE	21
	2. IDALIB	22
	3. BESSEL	22
	D. ERROR MESSAGES	22
	E. DETAILS OF JOB EXECUTION	23



VI.	PROGRAM MODE	27
A.	INPUTS	27
1.	TAPE5	27
B.	OUTPUTS	28
1.	Printouts	28
2.	Plots	28
C.	EXTERNAL REFERENCES	28
1.	INTMODE	29
2.	IDALIB	29
3.	BESSEL	30
D.	ERROR MESSAGES	30
E.	DETAILS OF JOB EXECUTION	30
VII.	EXAMPLES OF DISPERSION RELATIONS AND EIGENFUNCTIONS OBTAINED WITH INTMODE	33
	REFERENCES	47
	APPENDIX A - INTMODE SUBROUTINES	A-1

## I. INTRODUCTION

Generally, the numerical approach to finding internal wave eigenfunctions involves numerical integration of the differential equation over the entire ocean depth. For a deep ocean, particularly when the horizontal wavelengths of interest are much shorter than the ocean depth, numerical integration can be confined to the first few hundred meters of the ocean. This simplification arises from the fact that for a wide range of possible profiles the variation in depth dependence is confined to the upper few hundred meters below the surface, after which the profile may be approximated by a decaying exponential. Moreover, for horizontal wavelengths much shorter than the ocean depth the exponentially decaying profile model may be extended to infinity, i.e., the ocean may be assumed to have infinite depth. Since the solutions of the differential equation for a continuously decreasing exponential profile are known in closed form (they are Bessel functions of the first kind), numerical integration of the differential equation needs to be carried out only over the upper few hundred meters of depth, within which an essentially arbitrary Välsälä frequency profile may be prescribed, as derived from experimental data.

The numerical procedure to be presented here will provide any mode function and dispersion relation over any wavelength range for an arbitrary Välsälä frequency profile, as long as it decays exponentially at great depths. The practical limitation, of course, is the amount of computer time one is willing to expend for results covering an appropriate dynamic range. For ordinary ranges of physical interest, the required computing

time appears to be of the order of minutes for a dispersion curve and seconds for a mode function.

Dr. P. A. Selwyn, who was kind enough to review the first draft of this paper, has called attention to the fact that there already exists a computer program (Refs. 1 and 2) that performs calculations similar to those undertaken here, but for the case in which the ocean depth is finite. One would expect that it might have been possible to modify the earlier program so as to adapt it to the infinite depth case as well.

Although, in a sense, the question of that possibility was moot by the time this information had been disclosed, nevertheless, the option still exists for a potential user who, if convinced that the earlier program has sufficient advantages over the present one, might be willing to risk whatever numerical complications may be involved in such a task. Therefore, it seems proper to discuss briefly some of the major similarities and differences between the two programs. Unfortunately, a direct comparison of their computational accuracies and speeds is not feasible at present.\*

Both programs rely on the same general method, which is to start with the appropriate boundary condition at the deep end of the Väisälä frequency profile and numerically integrate the differential equation over depth for selected values of the wave number and phase velocity. These parameters are varied according to some iteration procedure until the value of the solution of the differential equation at the ocean surface is sufficiently close to zero.

The earlier program solves for the phase velocity in terms of the wave number. Here the converse is true.

---

\*If the adaptation of the earlier program were based on the same idea used here to account for the boundary condition at infinity, i.e., matching with the Bessel function solution for an exponential profile, the running time of the program would be increased considerably.

The earlier program uses a fourth-order Runge-Kutta method for solving the differential equation, so that the error is of fifth order in the incremental step size. Here the Numerov-Manning-Millman method is used, and the error is of sixth order in the incremental step size. This gain in efficiency occurs because the present method takes advantage of the fact that the differential equation does not contain a first derivative term.

The earlier program uses a Newton-Rapheson iteration scheme to find the eigenvalue, whereas here the *regula falsi* scheme is used. Generally, the Newton-Rapheson iteration converges faster but may fail to converge if the trial value is not sufficiently close to the true value. However, once started properly the *regula falsi* iteration is guaranteed to converge.\*

Other differences between the two programs primarily have to do with how they handle the problem of mode jumping, which occurs in the calculation when dispersion curves for successive modes approach each other too closely. The details are rather involved and it is difficult to assess the relative merits of the two approaches without considerable further study. However, it may be worth noting that the nature of the *regula falsi* method permits the use of certain eigenvalue properties, derived from the classical Sturm-Liouville theory, that aid in resolving the mode-jumping difficulties encountered by the program presented here.

The mathematical statement of the problem to be solved and some properties of the eigenfunctions and dispersion relations needed in the subsequent development are summarized in Chapter II. In Chapter III the general framework for the numerical

---

\*There are cases in which the convergence is extremely slow, however. When this happens it has been found expedient to switch to internal halving, which is less efficient, in general, but which converges at a predictable rate.

solution of the dispersion curves is presented. The detailed description of the algorithm for the numerical solution of the differential equation and the associated eigenvalues is given in Chapter IV. The computer implementation of this algorithm INTMODE is described in Chapters V and VI. A more detailed description is given in the Appendix.

Some examples of numerical results obtained with INTMODE are presented in Chapter VII.

## II. DESCRIPTION OF THE PROBLEM AND SOME GENERAL PROPERTIES OF INTEREST

Interest here is confined to internal waves with horizontal wavelengths of at most a few kilometers so that the effects of the inertial frequency do not enter. Accordingly, the mode functions  $\psi_m(y)$  are determined by the differential equation

$$\frac{d^2 \psi_m}{dy^2} + K^2 \left[ \frac{N^2(y)}{\Omega_m^2} - 1 \right] \psi_m(y) = 0, \quad (1)$$

along with the boundary conditions

$$\psi_m(0) = 0, \quad \lim_{y \rightarrow +\infty} \psi_m(y) = 0, \quad (2)$$

where the depth  $y$  is measured from the surface  $y = 0$ . In (1)  $K$  is a given wave number,  $\Omega_m$  is the mode frequency, and  $N(y)$  is the Väisälä frequency profile associated with a vertical thermocline in the ocean.

For a given value of  $K$  the differential equation (1) subject to the boundary conditions (2) determines uniquely the infinite set of mode functions  $\psi_m(y)$ . For each mode a dispersion relation is thereby determined; that is, each  $\Omega_m$  is a well defined function of  $K$ ,

$$\Omega_m = \Omega_m(K), \quad m = 1, 2, \dots, \quad (3)$$

over the interval

$$0 < K < \infty.$$

In general, the  $\Omega_m(K)$  are uniformly bounded, monotonic increasing functions that vanish at  $K = 0$ . As  $K$  becomes arbitrarily large each  $\Omega_m$  asymptotically approaches a single positive constant  $\Omega_0$  equal to the maximum value of  $N(y)$ , the Väisälä frequency. As  $K$  approaches zero the slope of each of the dispersion relation curves defined by (3) approaches a different finite positive value  $1/\mu_m$ ; i.e.,  $\lim_{K \rightarrow 0} \frac{d\Omega_m}{dK} = \lim_{K \rightarrow 0} \frac{\Omega_m}{K} = 1/\mu_m$ .

The dispersion relations (3) can be expressed parametrically in terms of a quantity  $\mu$ , which approaches  $\mu_m$  as  $K$  approaches zero; i.e.,

$$\begin{aligned} K_m &= K_m(\mu) \\ \Omega_m &= \frac{K_m(\mu)}{\mu}, \end{aligned} \quad (4)$$

where the set of functions  $K_m(\mu)$  are determined by the differential equation

$$\frac{d^2 \psi_m}{dy^2} + \mu^2 N^2(y) \psi_m = K_m^2 \psi_m, \quad (5)$$

subject to the boundary conditions (2). From this point of view, for each value of  $\mu$  that is chosen above the minimum value needed for the existence of the particular modes being considered, the boundary value problem determines a set of positive real eigenvalues\*  $K_m^2(\mu)$ , the square root of which provides the  $K_m(\mu)$ .

According to the general theory of eigenfunctions for the linear second order differential equation (Ref. 4), if  $N(y)$  is piecewise continuous, bounded and approaches zero as  $y$  becomes infinite, for fixed  $\mu$  there are a finite set of real positive eigenvalues  $K_m^2$ .\* As  $\mu$  increases, the number of these eigenvalues also increases, but for  $\mu$  smaller than some critical value there

---

\*Actually, the convention is to regard the quantities  $-K_m^2$  as the eigenvalues, which results in their being characterized as negative real.

may be no eigenvalues at all. It is also known from the general theory that each  $K_m$  is an increasing function of  $\mu$  (cf. Ref. 5, p. 357).

It is assumed that the Väisälä frequency profile  $N(y)$  decays exponentially at great depths. This behavior may be characterized more conveniently by actually requiring that after some depth  $y_0$ ,  $N(y)$  becomes an exponential function; i.e.,

$$N(y) = \hat{N}_0 e^{-\frac{y}{b}}, \quad y \geq y_0. \quad (6)$$

As observed in Ref. 1 the solution to the boundary value problem associated with (1) and (2) for an exponential profile of the form (6) is proportional to a function  $\phi(y)$  given by

$$\phi(y) = J_{Kb}(\mu b \hat{N}_0 e^{-\frac{y}{b}}). \quad (7)$$

Thus, the boundary conditions (2) can be restated as

$$\psi(0) = 0, \quad \psi(y) = A J_{Kb}(\mu b \hat{N}_0 e^{-\frac{y}{b}}), \quad y \geq y_0, \quad (8)$$

where  $A$  is a constant that can be chosen arbitrarily or to satisfy some normalization condition.

According to Ref. 3, a W.K.B. solution of (1) can be used to determine the approximate  $m^{\text{th}}$  mode dispersion relation; i.e., within the W.K.B. approximation the dispersion relation is determined by the equation

$$\int_{N > \Omega} p dy = \pi(m - \frac{1}{4}), \quad (9)$$

where

$$p(y) = \frac{K}{\Omega} [N^2(y) - \Omega^2]^{1/2} \quad (10)$$

$$= \sqrt{\mu^2 N^2(y) - K^2}.$$



### III. THE NUMERICAL PROCEDURE TO DETERMINE DISPERSION RELATIONS

In this chapter the principles underlying the numerical procedure to be used for calculating the dispersion relations will be outlined. The details of the procedure, itself, will be presented further on.

Since  $K$  is an increasing function of  $\mu$ , it follows from (9) and (10), by considering the limit as  $K$  approaches zero, that the minimum permissible value  $\mu_m$  for the  $m^{\text{th}}$  mode is given approximately by

$$\mu_m \sim \frac{\left(m - \frac{1}{4}\right)\pi}{\int_0^\infty N(y)dy} . \quad (11)$$

Since (11) is only an approximate formula, in order to guarantee that a solution  $K_m$  exists for the eigenvalue problem, values of  $\mu$  chosen to calculate the dispersion relation for a given mode should be somewhat larger; e.g., it would be prudent to confine the choice of  $\mu$  to values such that

$$\mu \geq \frac{\frac{3\pi}{2} + (m-1)\pi}{\int_0^\infty N(y)dy} . \quad (12)$$

The smallest value of  $\mu$  given by (12) ought to be large enough to guarantee the existence of a real  $K_m$  but, ideally, small enough to exclude the existence of any higher mode eigenvalue  $K_n$ ,  $n > m$ . It will be found that this is generally true but that there are some noteworthy exceptions.

For any choice of positive  $K$  and  $\mu$  it is possible to find a solution of the differential equation (5), subject to the second condition in (8) which determines the necessary initial values to be imposed for that purpose at the point  $y_0$ . The differential equation can be integrated numerically from  $y_0$  down to zero, where a value for  $\psi(0)$  will thus be acquired. If the maximum magnitude of the solution over the interval  $0 \leq y \leq y_0$  is  $|\psi_{\max}|$  then a function  $\Psi(\mu, K)$ , determined by this process, may be defined by

$$\Psi(\mu, K) = \frac{\psi(0)}{|\psi_{\max}|} . \quad (13)$$

As defined,  $\Psi(\mu, K)$  is a function of  $\mu$  and  $K$  alone; i.e., it is independent of the normalization constant  $A$ .\*

Because there are cases in which (12) does not lead to a satisfactory initial value for  $\mu$  (some modes are skipped) a slower but safer procedure than relying on the W.K.B. approximation has been adopted here. The differential equation (5) is solved numerically, subject to the second condition in (8), with  $K$  set equal to zero and  $\mu$  set equal to a sequence of values  $\frac{n}{\int_0^\infty N(y) dy}$ . For each value of  $\mu$  in the sequence the sign of  $\psi(0)$  is observed. When a change in the sign occurs the corresponding value of  $\mu$  is used as a trial value, and it is assumed that zero bounds  $K$  from below. If it is found that modes are still skipped, the  $\mu$  increment is decreased and the procedure repeated.

If  $K^2$  happens to be an eigenvalue, then  $\Psi(\mu, K)$  vanishes. Thus, the problem of calculating the dispersion relations is

---

\*Because it automatically relates error to a specified dynamic range, the normalization (13) is needed for stability of the numerical process used to solve (14).

equivalent to finding the real (positive) roots  $K(\mu)$  of the transcendental equation

$$\Psi(\mu, K) = 0 \quad (14)$$

as the parameter  $\mu$  varies. For sufficiently small  $\mu$  there are no roots, while for  $\mu$  in the interval

$$\mu_1 \leq \mu < \mu_2$$

there is just one root, and for  $\mu$  in the interval

$$\mu_2 \leq \mu < \mu_3$$

there are exactly two roots, etc.

To calculate the roots of (14), interval halving or, for more rapid convergence, the *regula falsi* (Ref. 6) method can be used. The numerical procedure given here does, in fact, rely upon the *regula falsi* method to solve (14), although the technique of interval halving is used in certain circumstances, to be described, in order to reduce computing time.

It is necessary to begin with two trial values for  $K(\mu)$ ,  $\tilde{K}_1$  and  $\tilde{K}_2 > \tilde{K}_1$ , such that  $\Psi(\mu, \tilde{K}_1)$  and  $\Psi(\mu, \tilde{K}_2)$  differ in sign, to guarantee that the root  $K(\mu)$  lies between  $\tilde{K}_1$  and  $\tilde{K}_2$ ; i.e.,

$$\tilde{K}_1 \leq K(\mu) \leq \tilde{K}_2 .$$

Since  $K(\mu)$  must be positive, initially, the trial value  $\tilde{K}_1$  can be zero. For the initial upper bound  $\tilde{K}_2$ , a quantity defined by

$$\tilde{K}_2 = N_{\max}^* \quad (15)$$

where  $N_{\max}$  is the largest value attained by  $N(y)$ , will suffice.

---

\*The fact that  $\tilde{K}_2$  as defined by (15) is an upper bound can be seen by multiplying (5) by  $\psi_m$  and integrating from 0 to  $\infty$ . Integration of the derivative term by parts shows that that term is negative.

For the higher modes it will again be necessary to begin with  $\tilde{K}_1 = 0$ . However,  $\tilde{K}_2$  may be set equal to the previously calculated value of  $K$  for the mode one step down at the same value of  $\mu$ . That is, since it is known that

$$K_{m-1}(\mu) > K_m(\mu),$$

in calculating  $K_m(\mu)$  a value for  $\tilde{K}_2$  given by

$$\tilde{K}_2 \leq K_{m-1}(\mu) \quad (16)$$

can be used.

As indicated, the trial value  $\tilde{K}_2$  should be slightly less than  $K_{m-1}(\mu)$  to avoid accidentally falling back onto the  $m-1^{\text{st}}$  mode dispersion curve because of normal errors to be expected in the calculation. A test should be included here to guarantee that the choice of  $\tilde{K}_2$  is not too much less than  $K_{m-1}(\mu)$ : the function  $\Psi(\mu, K)$  must change sign in going from  $\tilde{K}_1$  to  $\tilde{K}_2$ .\*

In order to obtain a trial value satisfying (16), it is necessary to have an estimate of  $K_{m-1}(\mu)$  that is known to be too small. Since it is generally not the case that  $K_{m-1}$  would have been calculated previously for exactly the value of  $\mu$  now encountered in the mode  $m$  calculations, the estimate of  $K_{m-1}(\mu)$  must be determined by interpolation, e.g., between values  $K_{m-1}(\mu_n)$  and  $K_{m-1}(\mu_n + \Delta\mu)$ , where

$$\mu_n < \mu < \mu_n + \Delta\mu.$$

However, if the  $K$  versus  $\mu$  curves are concave upward such an interpolation will produce an estimate that is too large; hence, the desired sign change in  $\Psi(\mu, K)$  would not occur. On the other

\*While the *regula falsi* method may still work even if this requirement is not met, it is not actually guaranteed to converge unless the sign change rule is imposed.

hand, a cruder, one-sided, interpolation that does guarantee the sign change can be used. That is, instead of interpolating between  $K_{m-1}(\mu_n)$  and  $K_{m-1}(\mu_n + \Delta\mu)$  the trial value estimate becomes

$$\tilde{K}_2 = \frac{K_{m-1}(\mu_n)}{\mu_n} \mu. \quad (17)$$

From the fact that  $\Omega_{m-1} = K_{m-1}(\mu)/\mu$  is a monotonic increasing function\* it can be readily inferred that  $\tilde{K}_2$  defined by (17) will, in fact, be smaller than  $K_{m-1}(\mu)$ .

Once  $K$  has been calculated for the initial choice of  $\mu$  for a given mode, the value of  $\mu$  is increased by adding a small increment  $\Delta\mu$ . A corresponding increment for the lower bound trial value  $\tilde{K}_1$  can be obtained from an interpolation analogous to (17).

That this can be done so that  $\tilde{K}_1$  continues to be a lower bound can be seen as follows. By definition,

$$K = \mu\Omega.$$

Therefore,

$$\frac{dK}{d\mu} = \Omega + \mu \frac{d\Omega}{d\mu}. \quad (18)$$

Although  $\Omega$  increases monotonically with  $\mu$ , it is uniformly bounded by the maximum Väisälä frequency; hence, the second term on the right of (18) approaches zero as  $\mu$  becomes arbitrarily large. This is evident in view of the fact that, since the derivative of  $\log \mu$  is  $\frac{1}{\mu}$ ,  $\frac{d\Omega}{d\mu}$  approaches zero faster than  $\frac{1}{\mu}$ . Then, for large enough  $\mu$ , according to (18),

$$\Delta K \sim \Omega \Delta \mu. \quad (19)$$

---

\*If it were not, a case of anomalous dispersion would be implied since, as already observed,  $K$  is an increasing function of  $\mu$ .

Moreover, because  $\Omega$  is a monotonic function of  $\mu$ , the estimate of  $\Delta K$  given by (19) is always too small.

Thus, the new  $\tilde{K}_1$  can be chosen in accordance with (19); i.e.,

$$\tilde{K}_1 = K_\mu + \Omega_\mu \Delta\mu = K_\mu + \Delta\mu \frac{K_\mu}{\mu}, \quad (20)$$

where  $K_\mu$  is the previously calculated value of  $K$  corresponding to the value of  $\mu$  before the increment  $\Delta\mu$  is added. For modes higher than the first ( $m = 1$ ) the use of (17) to obtain the upper bound  $\tilde{K}_2$  continues each time  $\mu$  is incremented, while the lower bound  $\tilde{K}_1$  is obtained from (20). For the first mode, however, (15) is the only estimate immediately available for the upper bound  $\tilde{K}_2$  as  $\mu$  is incremented, although (20) can still be used to estimate the lower bound  $\tilde{K}_1$ .

#### IV. DETAILS OF THE NUMERICAL PROCEDURE

##### A. SOLUTION OF THE DIFFERENTIAL EQUATION

The Numerov-Manning-Millman method (Ref. 6, pp. 204-205) is particularly convenient for solving (5) numerically for given values of  $\mu$  and  $K$ . The method requires two starting values; for a step size  $h$ ,  $\psi(y_0)$  and  $\psi(y_0+h)$  must be furnished initially. Then the differential equation can be integrated by means of a single recursion relation that involves only  $\psi$  and its second derivative, which is obtained from  $\psi$  and the relationship supplied by the differential equation, itself.

The starting values of  $\psi$  are obtained by recognizing that at  $y_0$  and  $y_0+h$  the profile  $N(y)$  is an exponential function of the form (6). Thus, in accordance with (7), at these points  $\psi(y)$  can be set equal to  $J_{Kb}(\mu b \hat{N}_0 e^{-\frac{y}{b}})$ .

When  $N(y)$  is prescribed numerically over an interval  $(0, y_0)$  the resolution of  $N(y)$  implies a limit on how small the step size  $h$  may be taken. Conversely, a natural limitation on how large  $h$  may be is the requirement that it be small compared to the minimum wavelength  $\lambda$  to be considered. Since the wavelength is given by

$$\lambda = \frac{2\pi}{K},$$

this means that the size of  $h$  is governed by the largest value to be considered for the wave number  $K$ .

## B. SOLUTION OF THE EIGENVALUE EQUATION

The eigenvalues  $K$  that determine the dispersion relation for each mode are found by solving (14) over an appropriate range of values for  $\mu$ . For this purpose the *regula falsi* method (Ref. 6, pp. 4-5) seems most effective.

In some cases, convergence of the *regula falsi* method is too slow. Therefore, if twenty iterations occur without satisfying the prescribed error criterion the computer program switches to interval halving with an error criterion applied to  $K$  rather than  $\psi$ .

## C. SELECTING INCREMENTS OF $\mu$

In accordance with (12), the increment  $\delta\mu$  used to obtain the starting value of  $\mu$  in going from the dispersion relation for one mode to that for the next is normally given by adding increments

$$\delta\mu = \frac{1}{\int_0^{\infty} N(y)dy} \quad (21)$$

until  $\psi(\mu, 0)$  changes sign. At the start of the mode,  $\tilde{K}_1$  is then set equal to zero.

If the increment  $\Delta\mu$  along a single mode is too large, a jump to the next mode may occur. This can be guarded against by calculating  $\psi(\mu + \Delta\mu, K_\mu)$  which in that case would have a different sign than  $\psi(\mu, \tilde{K}_1)$ , where  $\tilde{K}_1$  is a lower bound used in calculating  $K_\mu$ .

Evidently, as a practical matter  $\Delta\mu$  must not be too large. It is also true, however, that  $\Delta\mu$  must not be too small. While, theoretically, trial values are chosen so as to guarantee the necessary sign change in  $\Psi(\mu, K)$  for the *regula falsi* method, in practice it turns out that when  $\Delta\mu$  is sufficiently small the



sign change may, nevertheless, fail to occur. This is due to the residual calculation error in the  $K$  that corresponds to the value of  $\mu$  before it is incremented. This error is sufficient in some cases to overcome the theoretical inequality relied upon in the derivation of the rule for selecting  $\tilde{K}_2$ .

A compromise rule for selecting the  $\mu$  increment is to let  $\Delta\mu$  be about  $\frac{1}{10} \delta\mu$ . That is, a reasonable choice that seems adequate in practice is given by

$$\Delta\mu = \frac{1}{2 \int_0^\infty N(y) dy} . \quad (22)$$

#### D. ESTIMATING THE ERROR IN $K$

The test used to determine when to stop the *regula falsi* iterations in calculating  $K$  is the condition

$$|\Psi(\mu, K)| < \epsilon. \quad (23)$$

The value chosen for this purpose in current applications is  $10^{-7}$ , which is intended to provide at least a 60 dB dynamic range for the corresponding mode functions.

Therefore, the error in  $K$  is not given directly; however, it can be estimated by linear extrapolation. If  $\Psi_n$  is the value of  $\Psi(\mu, K)$  that just meets the test (23) and  $\Psi_{n-1}$  is the value of  $\Psi(\mu, K)$  in the iteration just before that one, then the quantity

$$\frac{\Delta K}{\Delta \Psi} = \frac{K_n - K_{n-1}}{\Psi_n - \Psi_{n-1}} \quad (24)$$

where  $K_n$  and  $K_{n-1}$  are the corresponding estimates of  $K$  in the two iterations, is approximately the rate of change of  $K$  with

respect to a change in  $\Psi(\mu, K)$ . Then the error  $\epsilon_K$  in  $K$  corresponding to  $\epsilon$  will be given approximately by

$$\epsilon_K = \frac{\Delta K}{\Delta \Psi} \epsilon. \quad (25)$$

The error estimate  $\epsilon_K$  can be used to prevent the anomaly mentioned earlier, that too small a choice of  $\Delta\mu$  can result in a failure to obtain a sign change in  $\Psi(\mu, K)$  using the trial value  $\tilde{K}_1$  obtained by means of (20). The idea is to make sure that the error in the calculated value of  $K$  is always negative, i.e., that the calculated value of  $K$  is too small. This can be done by subtracting  $\epsilon_K$  after the iterations for  $K$  are completed.

## V. COMPUTER REALIZATION OF THE ALGORITHM

The computer program DISPER was designed to calculate the  $K = K(\mu)$  relationship using the numerical techniques described earlier in this paper. This program will write the  $(K, \mu)$  pairs as calculated along each mode to disk or tape and will plot a graph of the  $(K, \Omega)$  curves, referred to as dispersion curves.

### A. INPUTS

The inputs to the program are of two types: (1) parameters read in under a NAMELIST option, and (2) data points read in from punched data cards.

#### 1. NAMELIST/PARAM/X0, B, STOPK, STOPMU, ND, EPS

X0	Real The X-coordinate of the last data point of the numerically defined function $N(X)$ . For the STD data $X0 = 220. \text{ m}$ .
B	Real Decay constant For the STD data $B = 1300$ .
STOPK	Real The maximum K value for which the user wants dispersion curves.
STOPMU	Integer The number of dispersion curves to be calculated.
ND	Integer The number of data points +1 to be read into the array N.

EPS

Real

The error criteria imposed on the numerical solutions to the differential equations. For the STD data EPS = 1.E-7.

## 2. Data Cards

ITITLE

Integer

Ten character title of the N(x) values.

N

Real array

Dimensioned 500, read in on punched cards under the format (8F10.5). N contains the equispaced data points that numerically define the function N(X). The points are spaced a distance of XO/(ND-2) apart.

## B. OUTPUTS

### 1. Printout

- a. The parameters defined by the NAMELIST option are listed at the end of the program for verification purposes.
- b. The value of  $\int N(y)dy$  is printed next, followed by the values of N.
- c. At the end of the calculations for each mode the number of (K, $\mu$ ) pairs, the maximum estimated error for K, and the complete list of (K, $\mu$ ) pairs for that mode are printed.
- d. Occasionally the error in K cannot be estimated. When that occurs a message indicating this fact and the current values of K and  $\mu$  are printed.

### 2. Disk or Tape

The values of the NAMELIST/PARAM/B, XO, STOPK, EPS, ND, STOPMU are written on TAPE2 under the format (4E22.7, 2I5//). Next the values of N are written to TAPE2 under the format (8E10.5).

At the end of each mode the number of  $(K, \mu)$  pairs calculated is written to TAPE2, format (//I5). The  $(K, \mu)$  pairs are then written to TAPE2, format (2E22.7).

TAPE2 may be defined as a permanent file by using a catalog control card, or it may be defined as a magnetic tape by using a label control card.

### 3. PLOT

A 10" by 10" graph consisting of the STOPMU different curves of the  $(K, \Omega)$  pairs is plotted at the end of the program.

## C. EXTERNAL REFERENCES

DISPER references several external subroutines that must be provided by the user through control cards that attach the appropriate permanent files.

The necessary routines are listed below under the name of the permanent file on which they reside.

### 1. INTMODE

INITIAL	Reads the data values of $N(X)$ , calculates the integral
---------	---

$$\int_0^{\infty} N(x) dx$$

GUESS	Calculates "best" estimate of $K$ given $\mu$ .
-------	---

DIFF	Numerically solves the differential equation using the Numerov-Manning-Millman method. Called by GUESS.
------	---

XMUØ	Function to find MUØ for each mode.
------	-------------------------------------

OUTPUTK	Writes the $(K, \mu)$ pairs to TAPE2.
---------	---------------------------------------

PLOTTER	Sets up the calls to the CalComp plotting routines.
---------	---

PSCALE	Scales the axes to the calculated data. Called by PLOTTER.
ERRPRO	Processes detected errors through a call to ABRTJOB. Is called by all of the routines on this permanent file.

## 2. IDALIB

PLOTS	CalComp plotting routines called by PLOTTER.
PLOT	
LINE	
DAXIS	
SYMBOL	
NUMBER	
ABRTJOB	Error processor that generates TRACEBACK, prints error messages, and terminates the job. Called by ERRPRO.

## 3. BESSEL

JBESS	Routines to calculate the BESSEL functions. Acquired from the Argonne National Laboratory.
JAIRY	
GAMLN	

## D. ERROR MESSAGES

We have attempted to anticipate some of the errors a user might encounter when using DISPER under very general conditions. If one of these errors is detected by the program the error processor ERRPRO is called. ERRPRO does three things, (1) prints a brief message describing the error, (2) indicates in which routine the error occurred, and (3) terminates the job without a dump.

A table of error messages generated by DISPER and possible corrective actions that might resolve the problem is presented below.

TABLE 1. ERROR MESSAGES AND POSSIBLE  
CORRECTIVE ACTIONS

Message	Significance	Action	Issued By
END-OF-FILE,UNITS	ND-1 is greater than the number of data points provided for N.	Decrease ND or provide more data.	INITIAL
INDEFINITE OPERAND 0/0	Solution to differential equation is inconsistent.	Look for coding errors in the routine DIFF.	DIFF
DIVISION BY ZERO	Algorithm for solving the differential equation has broken down.	Data points may be too far apart. Introduce more data, perhaps through interpolation.	DIFF
FIRST MODE CANNOT BE CONSTRUCTED	Cannot find MU0 for this mode.	Reexamine data.	XMU0
TOO MANY POINTS	More than 500 (K,u) pairs are need to construct this mode.	Decrease STOPK, or revise program by redimensioning SAVEK, SAVEMU, TEMPK, and TEMPMU.	DISPER
K1 and K0 ON SAME SIDE OF CURVE	Estimates for K are not upper and lower bounds.	<p>(1) Reduce EPS.</p> <p>(2) Reduce STOPMU or increase STOPK.</p>	GUESS

### E. DETAILS OF JOB EXECUTION

The following is a sample card deck for executing DISPER.

1.

```

IPU=TO*MT1. DRAWER=32375R
LABEL(PLONTAPE.WRITNG.L=NOCREPL0T.0=LN.X=CV.VSN=0)
ATTACH(RECEFL.MH=1.IN=PD)
ATTACH(INALIR.ID=CG)
ATTACH(NICORIN.ID=PD.MR=1)
MAP(OFF)
LOAD(DISPRIN)
LNSET(LIR=INALIM/RESEL/INTNODE)
EXECUTE.

```

[illegible]

6 7 8 9

For a permanent file the deck would contain two additional cards. The sample deck below is an example.

2.

```

IPU.T0.MT1. DRAPER.33375R
REQUEST(TAOF2.0MF)
LABEL(PLOTAPE.0.RTNG:L.NOCREFLOT,D=LO,X=C.V.VSN=0)
ATTACH(RECEFL.MN=1.IN=PD)
ATTACH(IDA1TR.10=C6)
ATTACH(NTSPIN.ID=PD.MR=1)
MAP(OFF)
LOAD(OISPRIN)
LNSET(LTR=TNALIN/RFSCEL/INTMODE)
EXECUTE.
CATALOG(TAOF2.UISPCUOVE.IN=PD)
7
8
9
PARAM X0=11.0.R=5.0.ND=177.ETOPK=.1,ETOPMU=22,EP0=1.F=75
PULSF

```

[illegible]

If the (K,μ) pairs are to be written to a magnetic tape the job stream might look like the example shown below:



3.

```

IPU,T0,MT2. DRAWER,3-3758
LABEL(PL0TAPF=0,RING,L=N0SREPL0T,D=L0,X=SV,VSN=0)
ATTACH(RESEFL,MN=i,I=PD)
ATTACH(IDA1IR,IU=CG)
ATTACH(0ISPRIN:ID=PA,M=1)
MAN(OFF)

LOAD(0ISPRIN)
LNSET(LI=FINAL I0/RESECL/INTMODE)
EXECUTE
LABEL(X,RING=I*UIPCIRAVE,X=SV,W=VSN=0)
REWIND(TAPE2)
COPY(TAPE2,X)
789
$PARA= X=111.085.0ND=177,STOPK=.1,ST0B=U=2A,F0
PULSF

```

[illegible]

Note the change in the job card as well as the additional control cards.

Should both a magnetic tape and a permanent file be desired the job stream would look like the next example.

4.

```

IPU,TQ,MT2,NDAPER,33375A
REQUEST(TAPE2,OFF)
LABEL(PL0TARF,w,RTAG,L=NO,REPL0T,D=L0,X=ev,VSN=0)
ATTACH(RESEL,MH=1,I=PN)
ATTACH(IDA,TR,ID=CG)
ATTACH(INIS,IN>ID=PA,MH=1)
MAN(OFF)
LOAD(DIAPRN)
LNSET(LIB=IDAI,LM/RESEL/INTMODE)
EXECUTE.
CATALOG(TAPE2,UISOCUNVE,I=PN)
LABEL(X,RTAG,I=INIS,PCUNVE,X=SV,W=VSN=0)
REWIND(TAPE2)
COPY(TAPE2,X)

```

[illegible]

## VI. PROGRAM MODE

The computer program MCDE was designed to calculate and plot the normalized mode functions  $\Psi(\mu, K)$ . Given (1) the dispersion curves created by DISPER, (2) a set of consecutive mode numbers, and (3) a value for K, this program will use the dispersion curves and linear interpolation to find the corresponding  $\mu$  values. It will then calculate and plot the mode function for each mode number.

### A. INPUTS

The inputs to this program are of two types: (1) the outputs of DISPER, and (2) a NAMELIST option.

#### 1. TAPE5

TAPE 5 is defined to be the disk file or magnetic tape produced by DISPER.

B,XØ,STOPK,EPS,ND,STOPMU

The first record on TAPE5 is the defining parameters used by DISPER to create the dispersion curves. They are read in under the format (4E22.7, 2I5//). For definitions see inputs to DISPER.

N

Empirical data, format (8F10.5). See Inputs to DISPER. There will be ND-1 values of N.

NPTS

Integer  
The number of (K, $\mu$ ) pairs for the current mode.  
Format (//I5).

K1, MU1

Real  
The K and MU values of  
each mode, (2E22.7).

STOPX

Real  
The depth to which the  
mode function is to be  
calculated. Must be  
greater than or equal to  
X0.

IFIRST

Integer  
The first mode to be  
calculated.

LAST

Integer  
The last mode to be cal-  
culated. All modes bet-  
ween IFIRST and LAST are  
calculated.

## B. OUTPUTS

### 1. Printouts

- a. The parameters defined by TAPE5 and the NAMELIST option are listed at the end of the program for verification purposes.
- b. N is listed.
- c. Mode number is printed followed by a list of PSI values for that mode. Format is (4E22.7).

### 2. Plots

10" by 10" graphs of the (X,PSI) values will be plotted, one plot for each mode.

## C. EXTERNAL REFERENCES

MODE references several external subroutines that must be provided by the user through control cards that attach the appropriate permanent files.

The necessary routines are listed below under the name of the permanent file on which they reside.

## 1. INTMODE

INITIAL

Reads the data values of  $N(X)$ ,  
calculates the integral

$$\int_0^{\infty} N(x) dx$$

DIFF

Numerically solves the differential equation using the Numerov-Manning-Millman method.

PSCALE

Scales the axes to the calculated data. Called by PLOTMODE.

ERRPRO

Processes detected errors through a call to ABRTJOB. Is called by all of the routines on this permanent file.

INTNP

Calculates the integral

$$\int_0^{\infty} N^2(x) \Psi^2(x) dx$$

FUNCT2

Calculates  $X * J(v, X)^2$ .  
Called by INTNP.

FUNCT4

Calculates the alternative asymptotic approximation for  $X * J(v, X)^2$ . Called by INTNP.

PLOTMOD

Sets up the calls to the CalComp plotting routines.

## 2. IDALIB

PLOTS  
PLOT  
LINE  
DAXIS  
SYMBOL  
NUMBER

CalComp plotting routines  
called by PLOTMOD.

ABRTJOB

Error processor that generates TRACEBACK, prints error messages, and terminates the job. Called by ERRPRO.

GAUSS

Numerical integrating routine using Gaussian quadrature. Called by INTNP.

### 3. BESSEL

JBESS

JAIRY

GAMLN

Routines to calculate the BESSEL functions. Acquired from the Argonne National Laboratory.

### D. ERROR MESSAGES

A table of error messages generated by MODE and possible corrective actions that might resolve the problem is presented below.

TABLE 2. ERROR MESSAGES GENERATED BY MODE  
AND POSSIBLE CORRECTIVE ACTIONS

Message	Significance	Action	Issued By
More than 500 pairs were needed for this mode.	DISPER was altered to permit more than 500 pairs to be calculated.	Make similar changes in MODE.	MODE
The maximum K value on TAPES is less than the K of interest.	The dispersion curves were not calculated to this value of K.	Rerun DISPER with STOPK greater than K, or reduce value of K.	MODE
There are not enough modes on TAPES.	STOPMU is less than LAST.	Reduce LAST to less than STOPMU, or rerun DISPER with STOPMU greater than LAST.	MODE
Indefinite operand 0/0	Solution to differential equation is inconsistent.	Look for coding errors in the routine DIFF.	DIFF
Division by Zero	Algorithm for solving the differential equation has broken down.	Data points may be too far apart. Introduce more data, perhaps through interpolation.	DIFF

### E. DETAILS OF JOB EXECUTION

The following is a sample card deck for executing MODE, when the dispersion curves are on a permanent file.

```

IPD*MT1, DRAPER, 325/54
ATTACH(MODE, IU=PU)
FTN(I=MODE, L=U)
MAP(OFF)
ATTACH(INTMODE, IU=PI)
ATTACH(BESSEL, IU=PI)
ATTACH(IDALIM, IU=CU)
LABEL(PLOTAPF, *MINIS, L=NUSHEPLUT, D=LU, X=SV, VSN=U)
LDSET(LIB=INTMODE/BESSEL/IDALIB)
LGO.

```

739

```

$INPUT IFIRST=1, LAST=2, N=.02, STOPX=250.5

```

6789

Next is a sample card deck for executing MODE when the dispersion curves are on a magnetic tape. Note the VSN number should be the one assigned at the time DISPER executed.

```

IPD*MT1, DRAPER, 325/54
ATTACH(MODE, IU=PU)
FTN(I=MODE, L=U)
MAP(OFF)
ATTACH(INTMODE, IU=PI)
ATTACH(BESSEL, IU=PI)
ATTACH(IDALIM, IU=CU)
LABEL(TAPES, *NORINIS, L=DISPCURVE, VSN=5555)
LABEL(PLOTAPF, *MINIS, L=NUSHEPLUT, D=LU, X=SV, VSN=U)
LDSET(LIB=INTMODE/BESSEL/IDALIB)
LGO.

```

789

```

$INPUT IFIRST=1, LAST=2, N=.02, STOPX=250.5

```

6789

## VII. EXAMPLES OF DISPERSION RELATIONS AND EIGENFUNCTIONS OBTAINED WITH INTMODE

The two Väisälä frequency profiles considered in the sample calculations employing INTMODE are shown in Fig. 1. The profile labeled "exponentially stratified ocean" corresponds to a deep ocean without a thermocline and  $N(y) = .00528 \exp - y/1300$  radian/sec, where  $y$  is in meters. This profile is identical to the one used by Garrett and Munk (Ref. 7). For the exponential Väisälä frequency profile, the mode functions are Bessel functions. Consequently, results of INTMODE for this profile can be compared with results based on analytical formulae, thus providing a check on the accuracy of the numerical technique. The sharp thermocline, labeled "STD data set", is taken from (Ref. 8) and is based on measured towed thermistor chain data in the tropical Pacific Ocean. The data extends to a depth of 220 meters; at greater depths an exponential profile with a decay constant of 1300 meters is assumed.

The dispersion curves for the first 25 modes, corresponding to the STD data set, are plotted in Fig. 2. The angular frequency is in radians/sec. For the STD data set, plots of the first four internal wave modes are shown in Fig. 3 for  $K = .01$  radians/meter ( $\lambda \approx 628\text{m}$ ) and in Fig. 4 for  $K = .02$  radians/meter ( $\lambda \approx 328\text{m}$ ). The mode functions are all normalized in accordance with

$$\int_0^{\infty} \psi^2(y) N^2(y) dy = 1.$$

Since  $N(y)$  decays exponentially with depth, this normalization constraint leads to a progressive increase of the mode maximum with mode number and depth, a feature corroborated by the plots in Figs. 3 and 4.



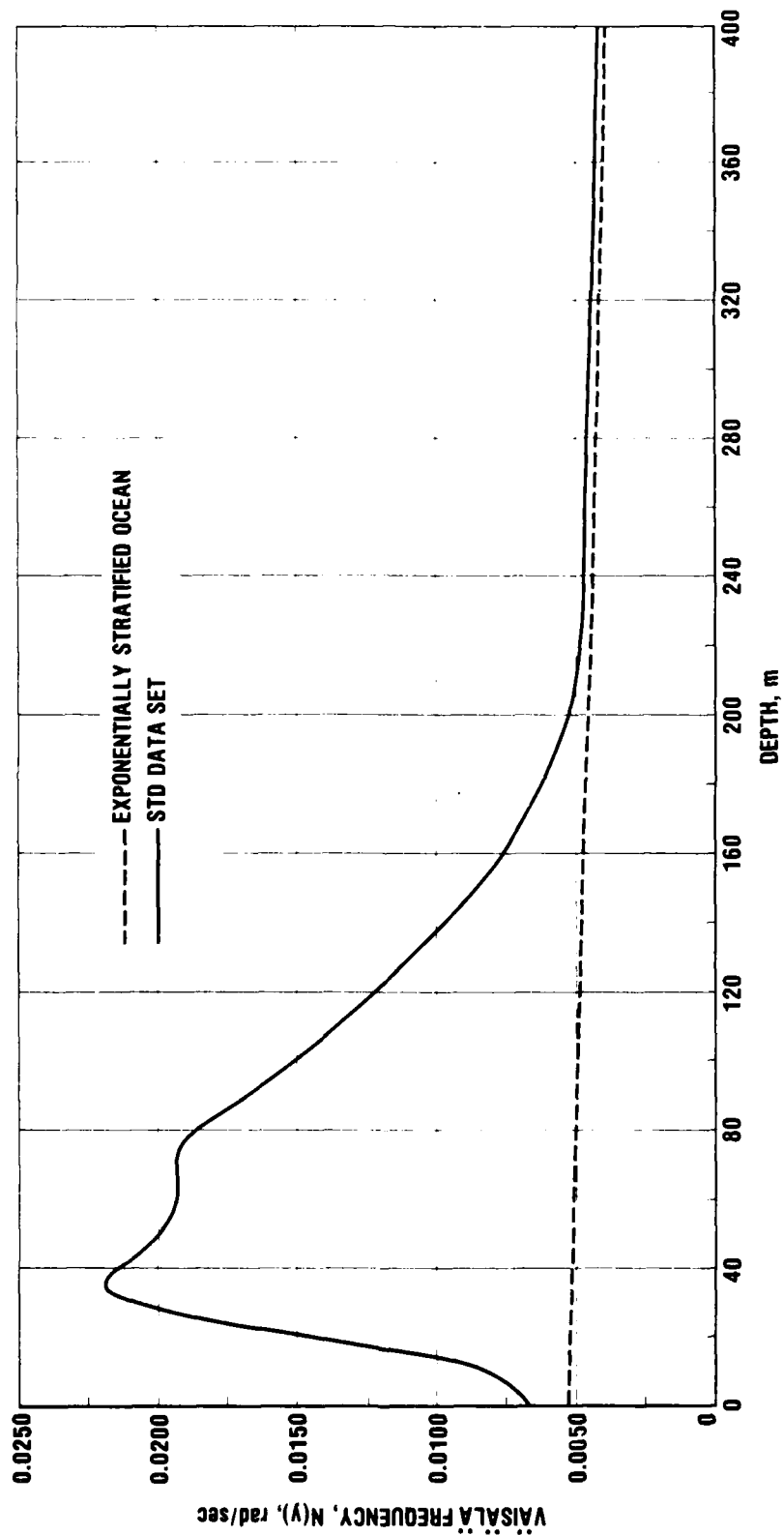
INTMODE is capable of yielding mode functions of any order (subject to course to the resolution of the data with respect to depth. Figure 5 shows a plot of the 25th mode.

The dispersion relations for the exponential profile are shown in Fig. 6; the first four mode functions are shown in Fig. 7 and Fig. 8, for  $K = .01$  and  $K = .02$  radians/meter, respectively.

Examples of dispersion relations for other profiles are shown in Figs. 9 and 10. The corresponding profiles are, respectively, those referred to in Fig. 12 as STD data and NRL data. An additional example of dispersion relations, corresponding to a pulse shaped profile, is shown in Fig. 11. This profile is of the form

$$\begin{aligned} N(y) &= 0; & 0 < y < 65.45\text{m}, \\ N(y) &= .0105 \text{ rps} & 65.45\text{m} < y < 111\text{m} \\ N(y) &= 0; & y > 111\text{m}. \end{aligned}$$

In the region  $y < 111\text{m}$   $N(y)$  was approximated by the rapidly decaying exponential  $\exp - y/5$ .



12 17 79.3

FIGURE 1. Väisälä frequency profiles used in the calculation of internal wave mode functions and dispersion relations.

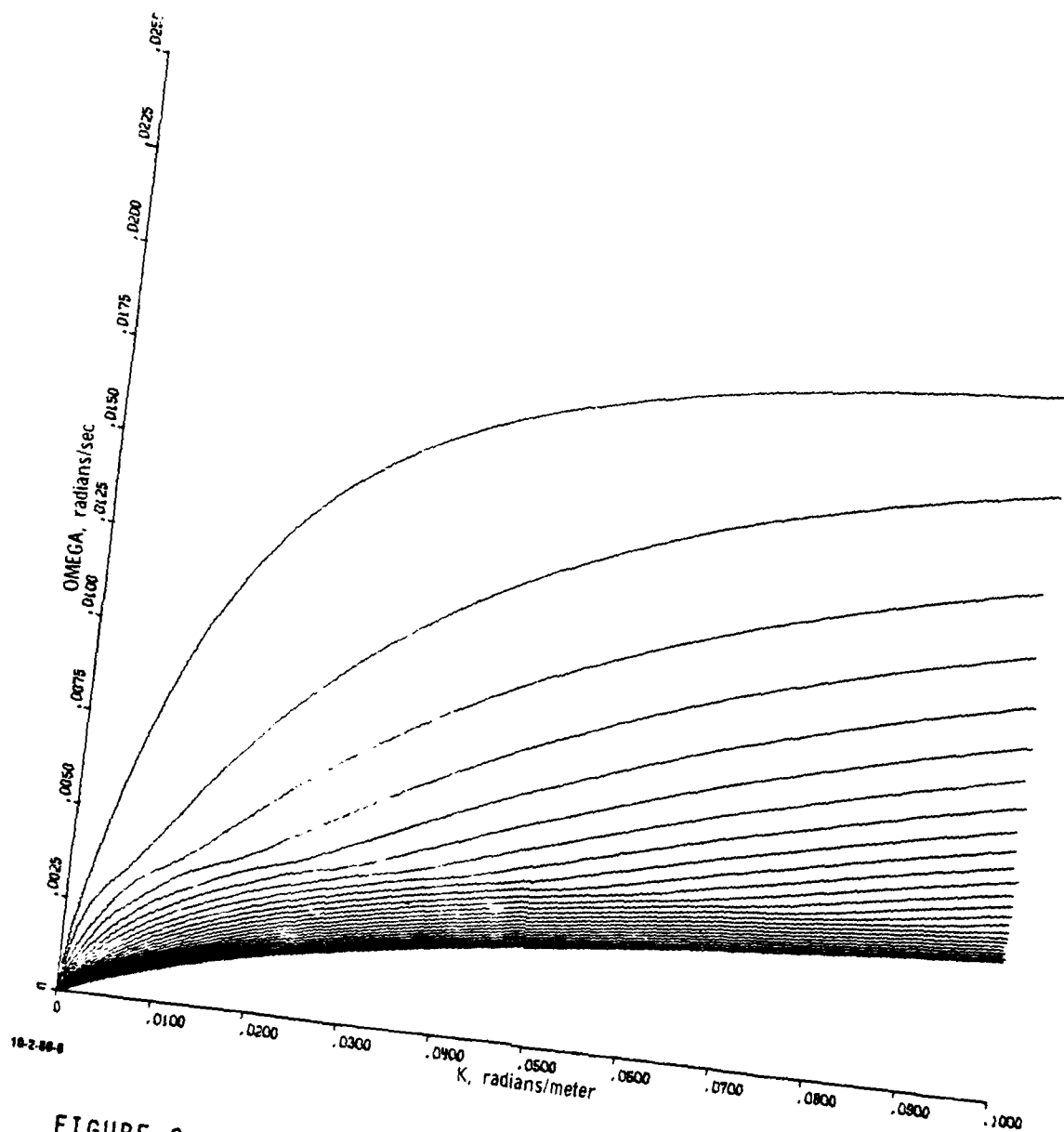
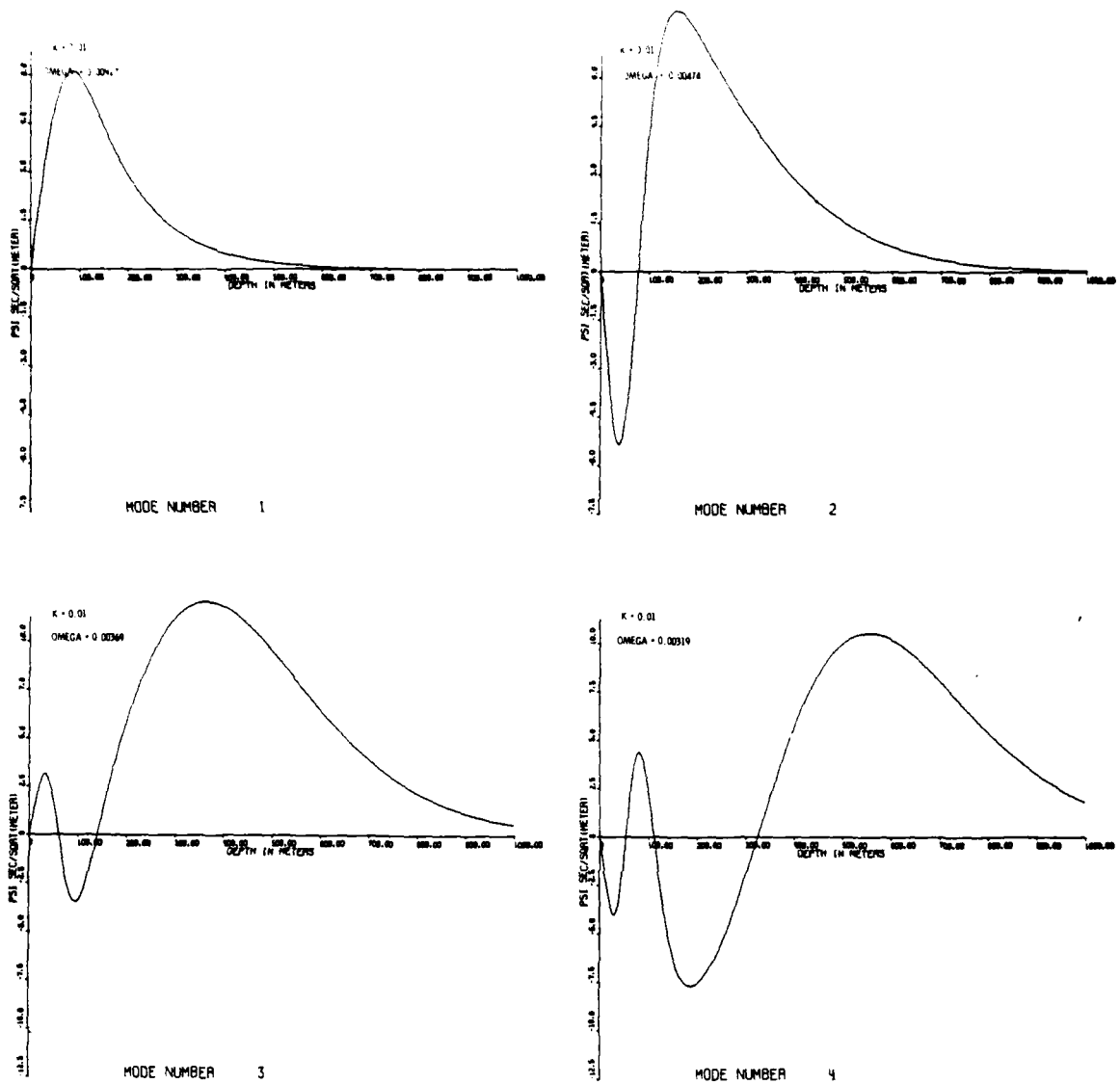
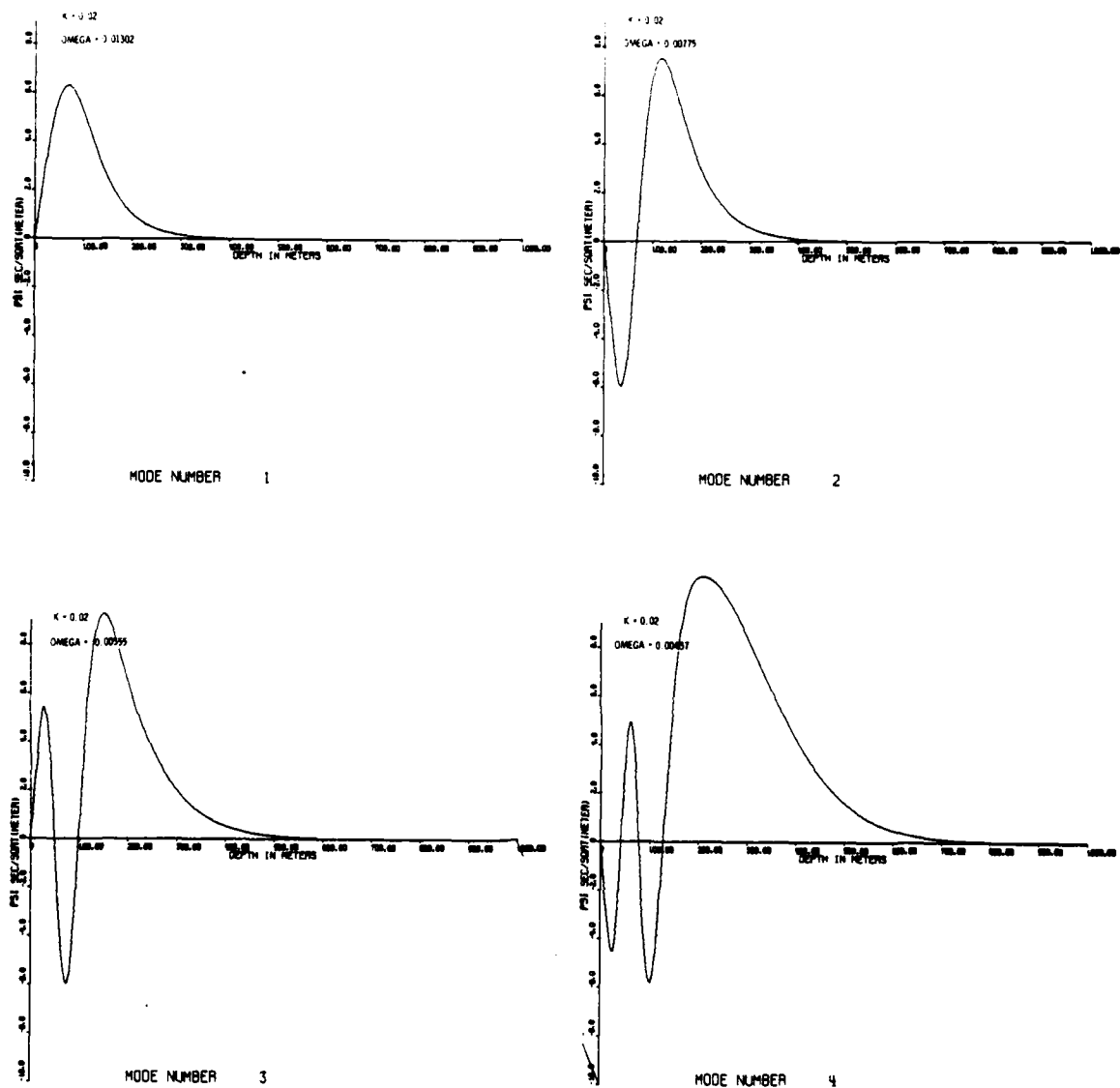


FIGURE 2. Internal wave mode dispersion curves for the Väisälä frequency profile corresponding to the "STD data set" in Fig. 1.



10-2-80-9

FIGURE 3. The first four internal wave modes for the STD data set (Fig. 1) ( $\lambda \approx 628$  meters).



18-2-88-10

FIGURE 4. The first four internal wave modes for the STD data set (Fig. 1) ( $\lambda \approx 314$  meters).

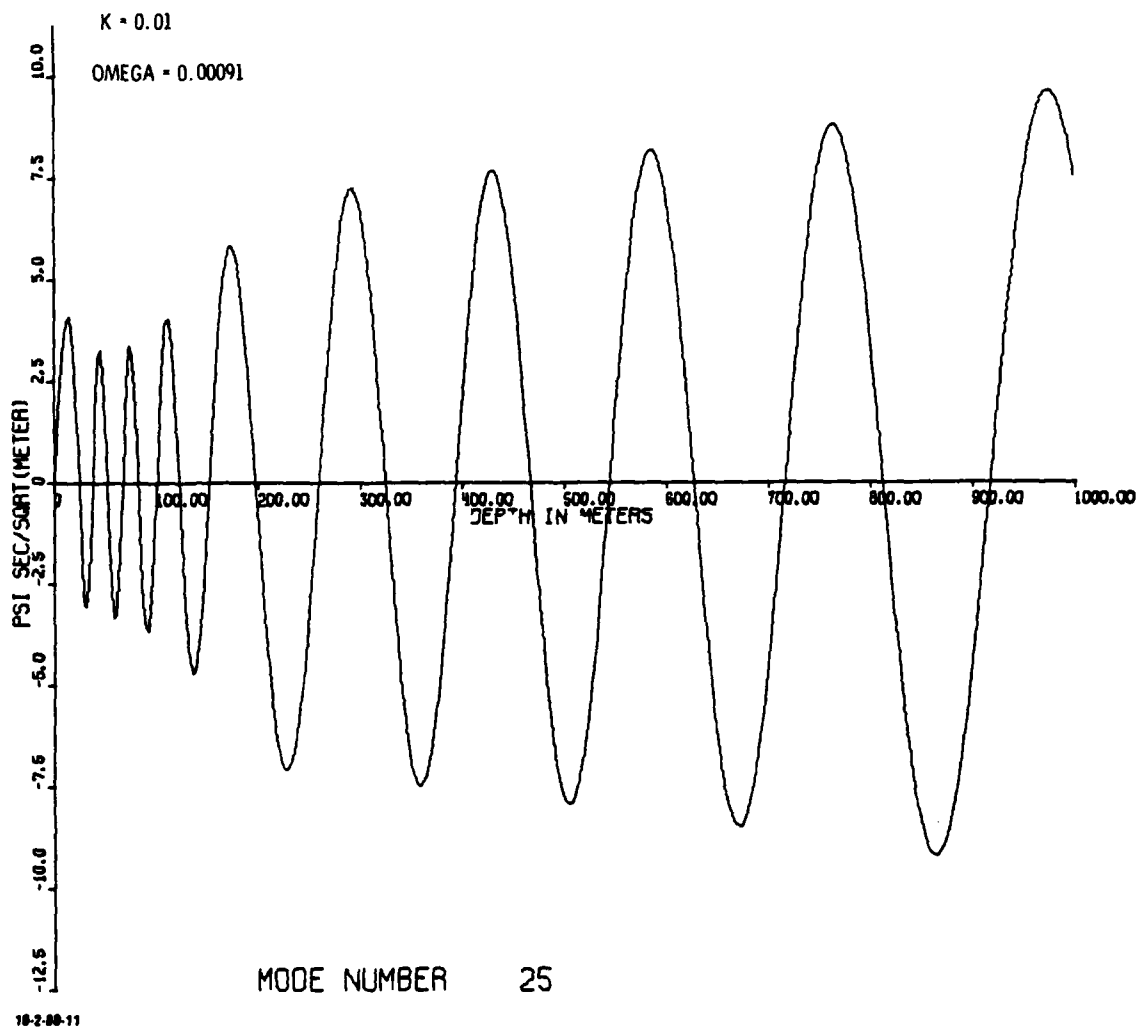


FIGURE 5. The 25th mode for the STD data set ( $\lambda \approx 628$  meters).

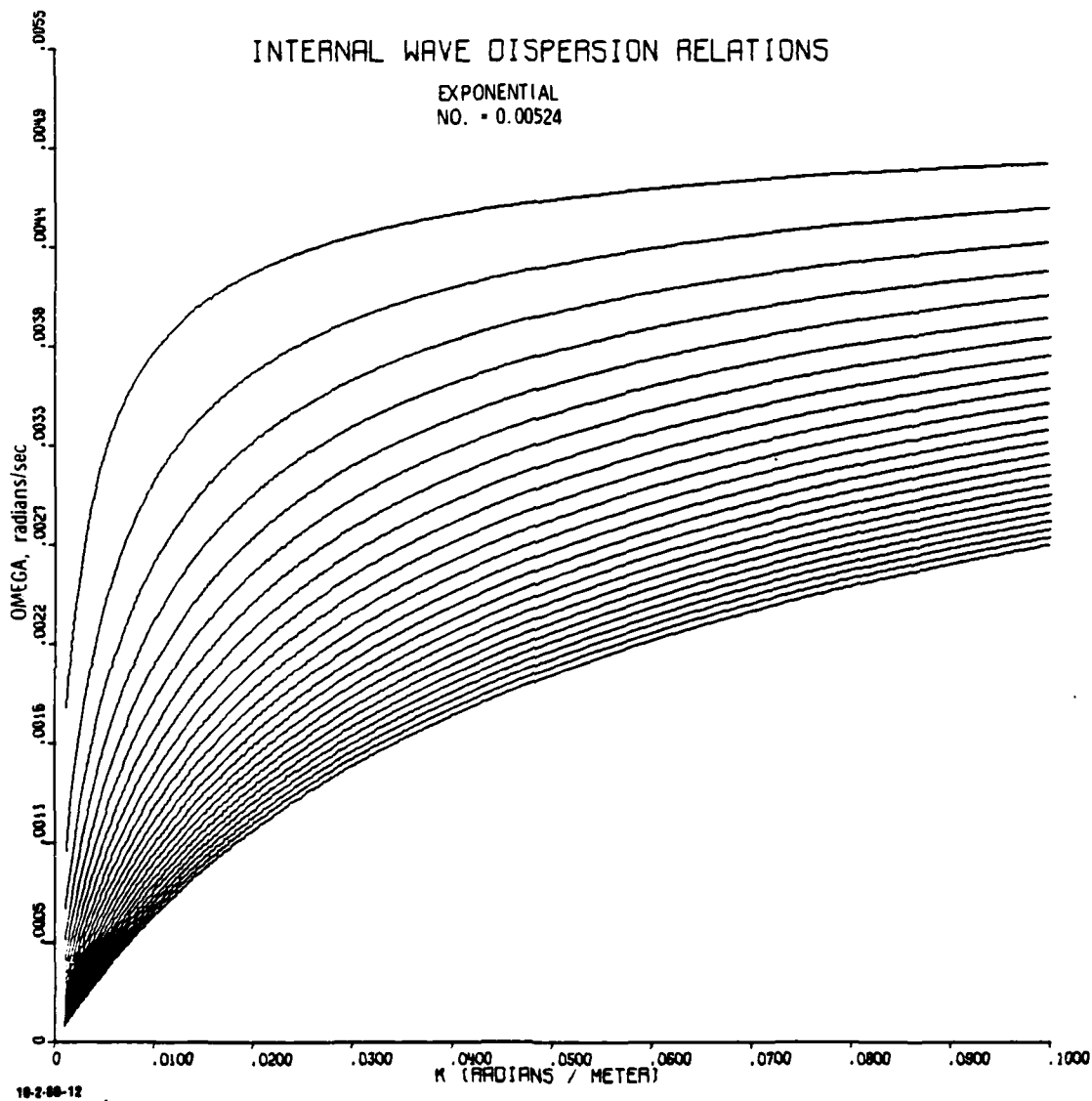
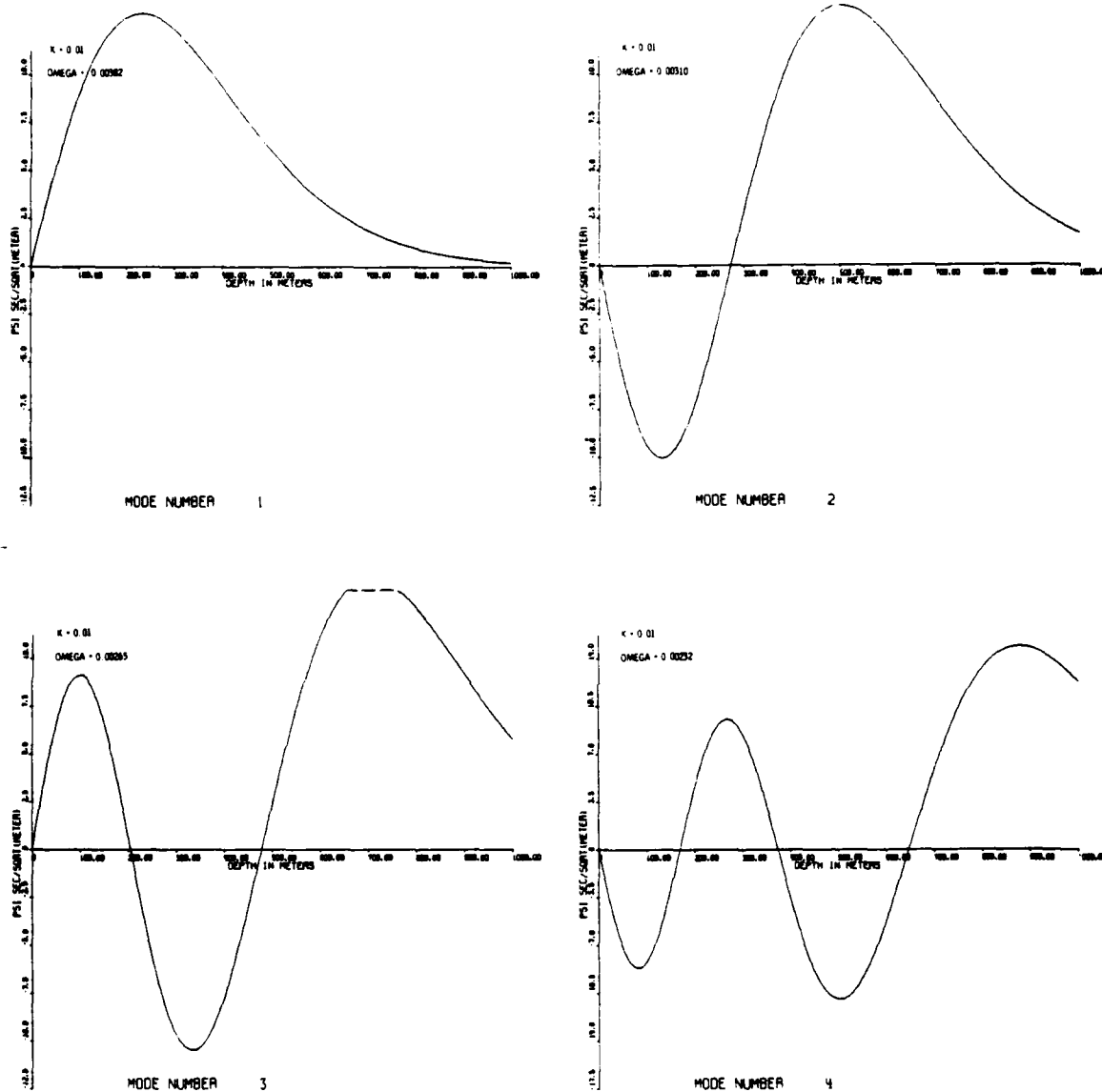


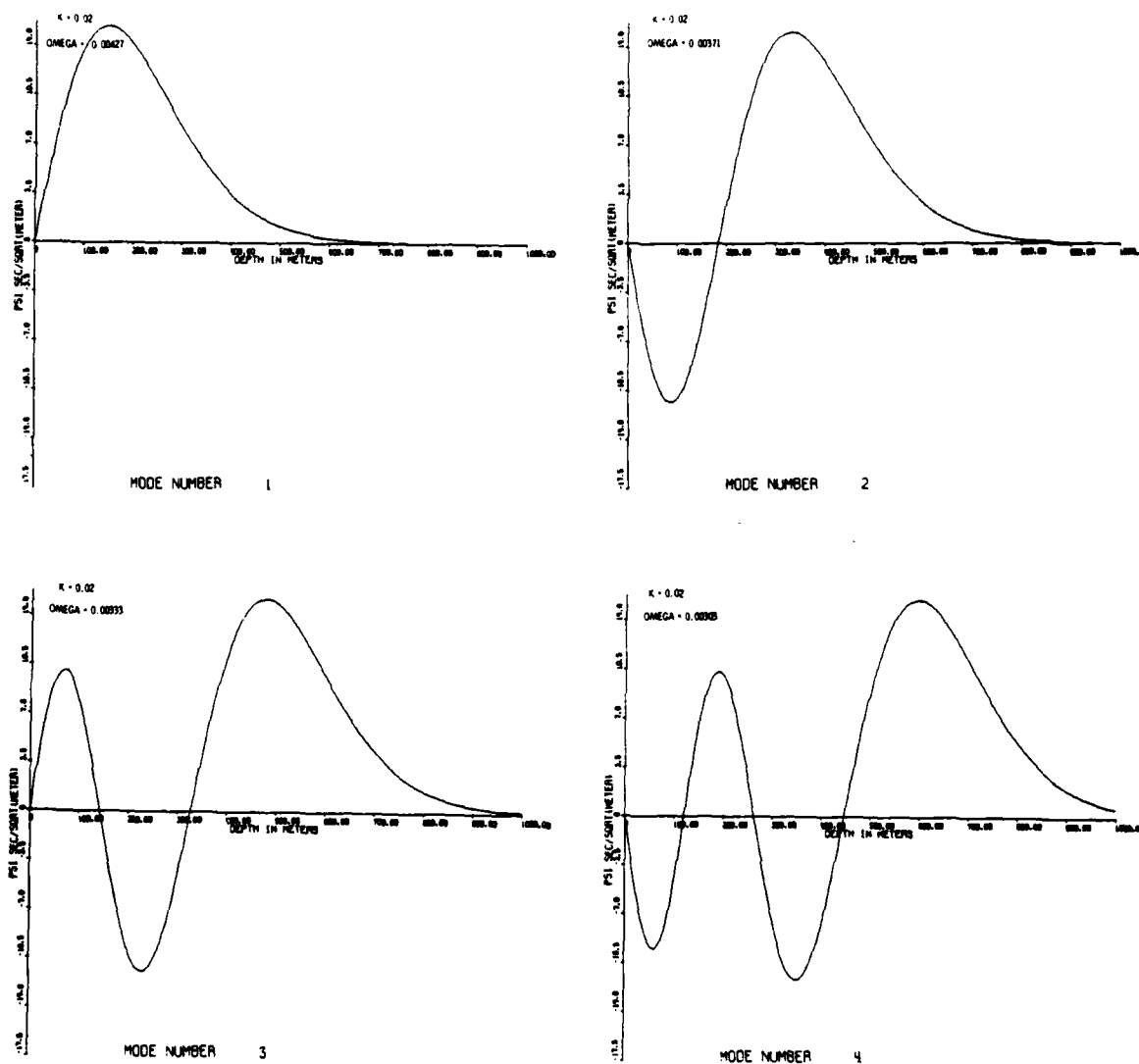
Figure 6. Internal wave mode dispersion curves for an exponentially decreasing Väisälä frequency profile.



10-2-66-13

FIGURE 7. The first four internal wave modes for the exponentially decreasing Väisälä frequency profile ( $\lambda \approx 628$  meters).





10-2-66-14

FIGURE 8. The first four internal wave modes for the exponentially decreasing Väisälä frequency profile ( $\lambda \approx 314$  meters).

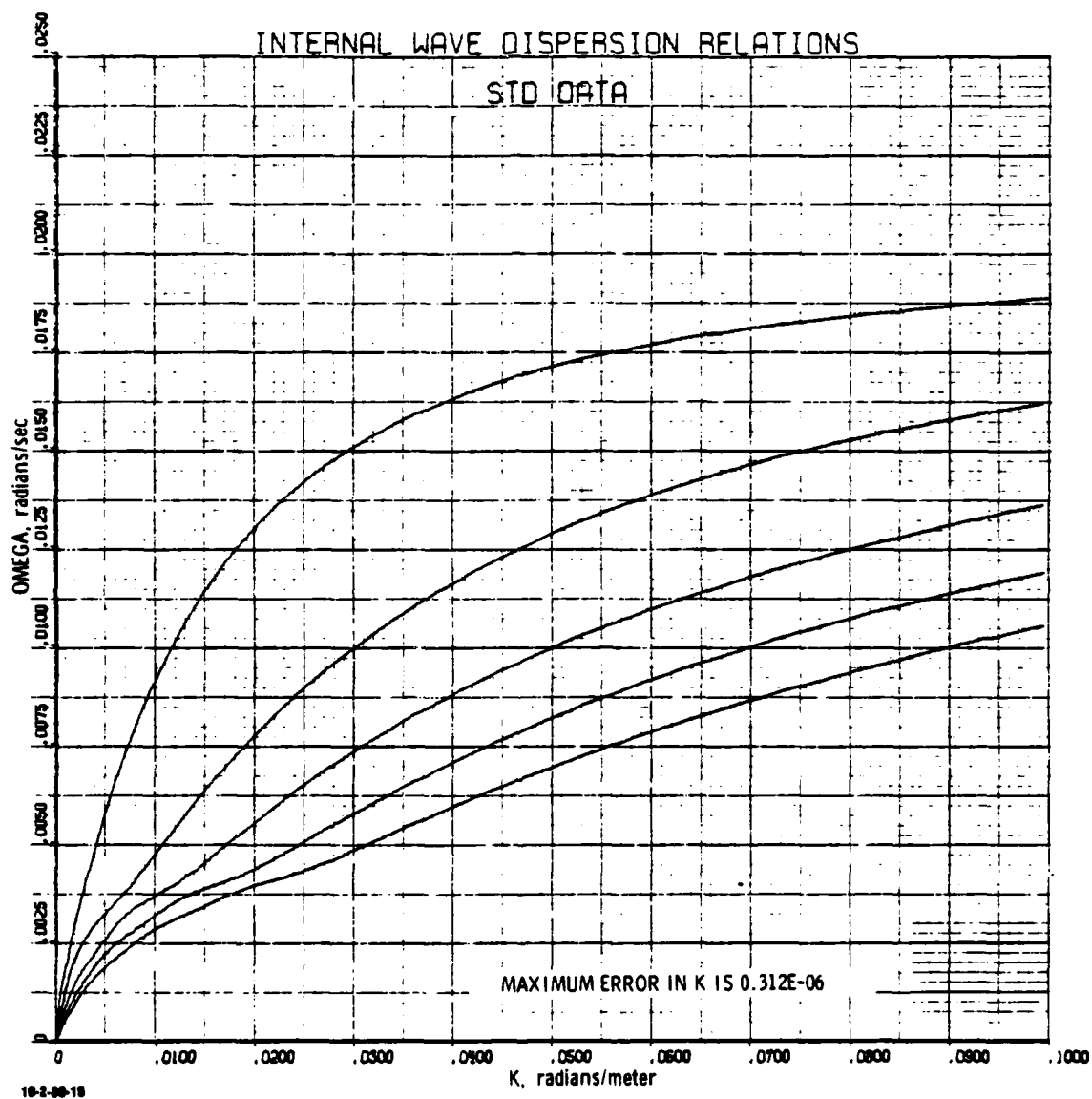


FIGURE 9. Internal wave dispersion relations -- STD data.

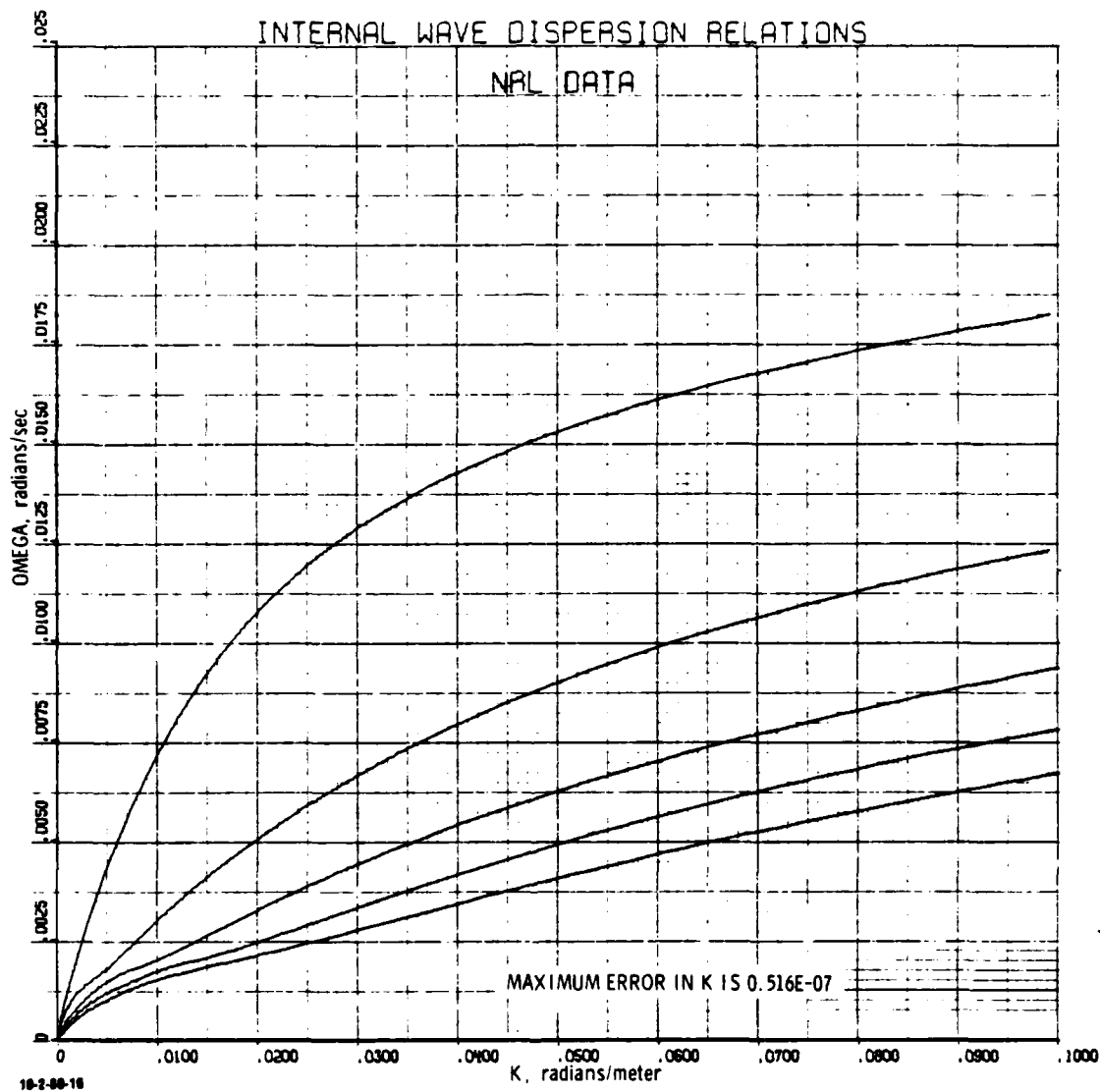


FIGURE 10. Internal wave dispersion relations -- NRL data.

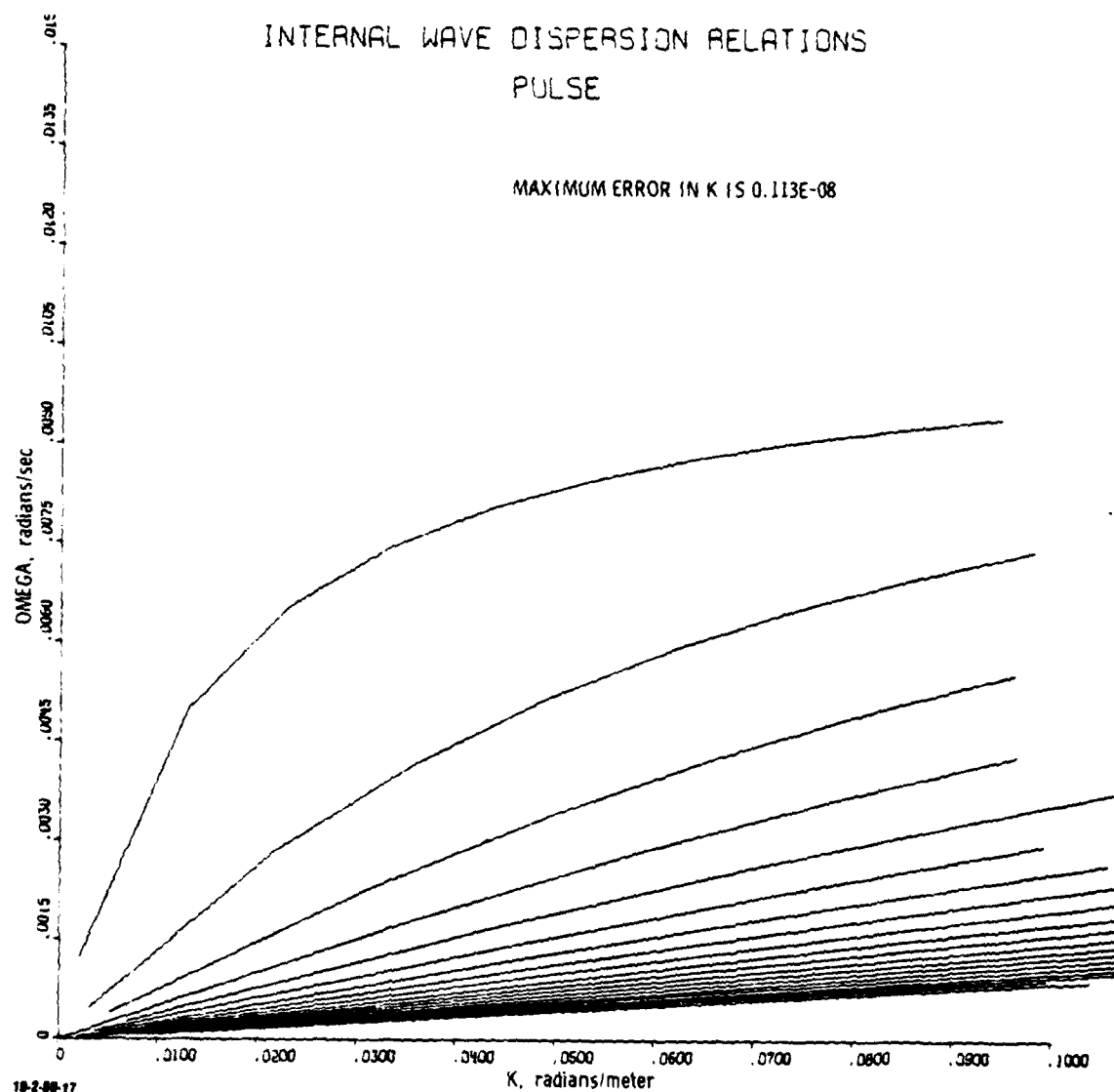


FIGURE 11. Internal wave dispersion relations -- pulse.

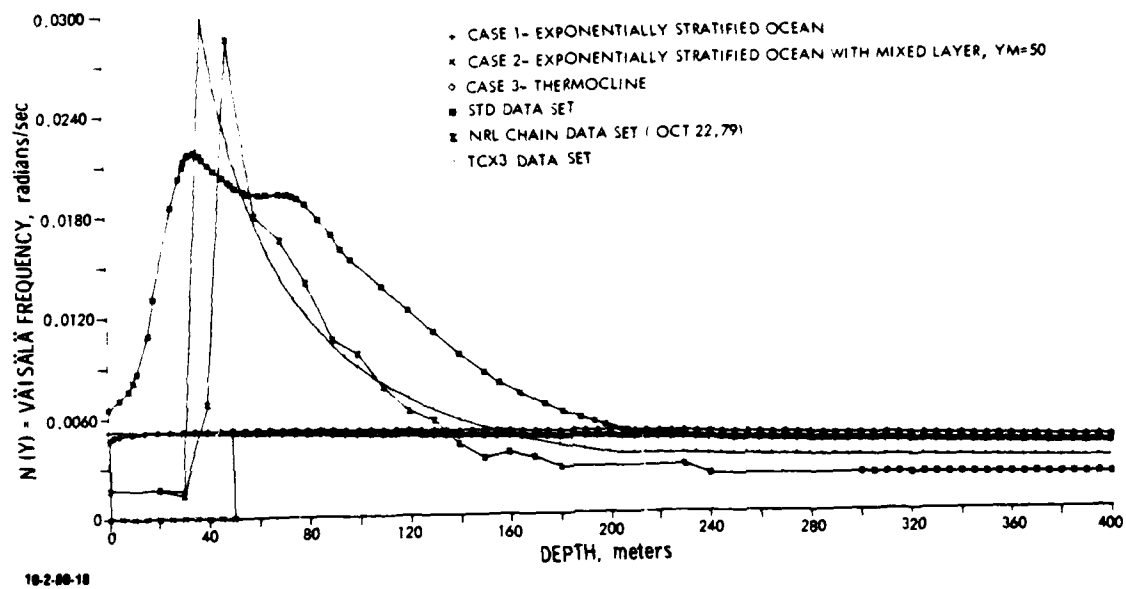


FIGURE 12. Väisälä Frequency Profiles.

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## APPENDIX A

### INTMODE SUBROUTINES

#### Contents

Subroutine:	DISPER	A-3
	XMUØ	A-10
	GUESS	A-11
	MODE	A-14
	DIFF	A-18
	INTNP	A-19
	FUNCT 2	A-20
	FUNCT 4	A-21
	INITIAL	A-22
	OUTPUTK	A-23
	ERRPRO	A-24
	PLOTMOD	A-25
	PLOTERR	A-26
	PSCALE	A-27

```

1      *DECK DISPER
      PROGRAM DISPER(INPUT,OUTPUT,TAPE2,TAPE3,IAPE5=INPUT)
3
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C
59     C
60     C
61     C
62     C
63     C
64     C
65     C
66     C
67     C
68     C
69     C
70     C
71     C
72     C
73     C
74     C
75     C
76     C
77     C
78     C
79     C
80     C
81     C
82     C
83     C
84     C
85     C
86     C
87     C
88     C
89     C
90     C
91     C
92     C
93     C
94     C
95     C
96     C
97     C
98     C
99     C
100    C

```

\*\*\*\*\*

A CDC 6400 SUBROUTINE

PROGRAMMER  
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DISPER CALCULATES AND GRAPHS DISPER-  
SION CURVES ACCORDING TO NUMERICAL  
TECHNIQUES DEVELOPED BY DR. I. KAT  
AND W. WASYLKIWEKIJ OF IDA

PROBLEM  
GIVEN A FUNCTION  $N(x)$  DEFINED  
NUMERICALLY FROM  $x = 0$  TO  $x = x_0$  AND  
BY THE RELATION

$$N(x) = N_0 \cdot \exp(-(x - x_0) / R)$$

FOR  $x \geq x_0$  AND A DIFFERENTIAL  
EQUATION

$$D^2(PST)/n(x)^2 =$$

$$(K^2 - MU^2 \cdot N(x)^2) \cdot PST$$

WITH PARAMETERS MU AND K THAT TAKE  
ON VARIOUS REAL VALUES

IT IS KNOWN THAT IN THE REGION WHERE  
 $x \geq x_0$  THAT ONE SOLUTION OF THE  
DIFFERENTIAL EQUATION IS THE BESSEL  
FUNCTION WITH INDEX  $k = R$  AND ARGU-  
MENT  $MU \cdot R \cdot N_0 \cdot \exp(-(x - x_0)/R)$

BY VARYING THE PARAMETERS MU AND K

ONE CAN FIND DIFFERENTIAL EQUATIONS, ONE OF  
WHOSE SOLUTIONS MATCH THE BESSEL  
FUNCTION SOLUTION WHEN  $x \geq x_0$  AND  
ALSO VANISH AT  $x = 0$ .

THIS PROGRAM DETERMINES THE RELATION  
 $k = k(MU)$   
THAT PROVIDES JUST SUCH DIFFERENTIAL  
EQUATIONS

IT THEN GRAPHS  $(k / MU)$  VS.  $k$

\*\*\*\*\*



```

C      *
C      * DESCRIPTION OF ARGUMENTS
60 C      * THE FOLLOWING PARAMETERS ARE
C      * MEMBER OF THE NAMELIST GROUP
C      * CALLED PARAM
C      * X0      REAL
C      *          THE X-COORDINATE OF THE
65 C      *          LAST POINT OF THE NUMERICAL
C      *          DATA
C      *
C      * B      REAL
C      *          THE DECAY CONSTANT
70 C      *
C      * ND      INTEGER
C      *          THE NUMBER OF NUMERICALLY
C      *          DEFINED POINTS + 1
C      *
75 C      * STOPK   REAL
C      *          THE MAXIMUM K VALUE TO BE
C      *          CALCULATED FOR EACH MODE
C      *
C      * STOPMU   INTEGER
80 C      *          THE NUMBER OF MODES TO BE
C      *          CALCULATED
C      *
C      * EPS      REAL
85 C      *          ERROR CRITERIA IMPOSED ON
C      *          THE SOLUTION TO THE DIFFERENTIAL EQUATION
C      *
C      *
C      * THE LAST INPUTS TO THE PROGRAM ARE
90 C      * THE NUMERICAL VALUES THAT DEFINE
C      * N(X) FROM 0 TO Y0. THEY ARE READ
C      * FROM CARDS. THE VALUES MUST BE 40
95 C      * PLUMPED AS TO BE READ UNDER THE
C      * FORMAT(=F10.5)
C      *
C      * N      REAL ARRAY
C      *          DIMENSION 500
100 C      *
C      * *****
C
105 C      COMMON/INPUTS/R,ND,X0,EPS,STOPMU,STOPK,STOPE
C      COMMON PST(500),N(500),ND,DELTA,NT,ITITLE
C      COMMON /OUT/ SAVEK(500),SAVEMU(500)
C      DIMENSION TEMPK(500),TEMPMU(500)
C      REAL N,N0,MU,K0,KMAX,MU0,K1
C      INTEGER STOPMU
110 C      NAMELIST/PARAM/R,ND,Y0,STOPMU,STOPK,EPS
C      MODE = 1
C      FORMAX = N0
C      PT = ACOS(-1.)
C      IERR = 6

```

PROGRAM NISPEC

```

115      C      READ PARAMETERS
      C
      C      S READ PARAM
      C      PRINT PARAM
120      C      READ NUMERICAL VALUES FOR N AND INTEGRATE N
      C
      C      CALL INITIAL(SUM1)
      C      PRINT 7000, SUM1
125      7000  FORMAT(*,SUM1*,*,F22.7)
      C      PRINT 100,(N(I),I=1,ND)
      C
      C      WRITE NAMELIST AND N TO TAPE2
130      C
      C      CALL OUTPUTK(1)
      C      FIND MAXIMUM VALUE FOR N
      C
135      C      KMAX=N(1)
      C      DO 10 I=2,ND
      C      10  KMAX=AMAX1(KMAX,N(I))
      C
      C      CALCULATE MU0 FOR THE FIRST BRANCH
140      C      NY = .1/SUM1
      C      MU0 = XMUN(0.,NY)
      C
      C      CALCULATE INITIAL ESTIMATE FOR THE INCREMENT IN MU
      C      ALONG A MU0 BRANCH
145      C
      C      TDELTA = .5 / SUM1
      C      XDELTA = TDELTA
      C
      C      START THE PROCESS OF APPROXIMATING K
150      C
      C      K0 = 0.
      C      MU=MU0
      C      KOUNT = 0
      C      200  CONTINUE
155      C
      C      CALCULATE THE UPPER ESTIMATE OF K,K1
      C
      C      K1 = MU + KMAX
      C
160      C
      C      CALL SUBROUTINE GUESS TO IMPROVE THE ESTIMATE K
      C      K1 IS UPPER ESTIMATE. K2 IS LOWER ESTIMATE. THE
      C      IMPROVED ESTIMATE IS RETURNED IN K1.
      C
165      C
      C      CALL GUESS(K0,K1,MU)
      C
      C
170      C      CHECK FOR ERROR CODES RETURNED IN NT
      C
      C

```

PROGRAM DISPEN

```

C      NT = 9          INDICATES THE ALGORITHM COULD NOT PRO-
C                      DUCE A K FOR MU0 ON THE FIRST BRANCH.
C                      K1 IS NOT ABOVE THE CURVE.
175  C
C      IF (NT .EQ. 9) CALL ERRPRN(5)
C
180  C
C      THE MAXIMUM ESTIMATED ERROR FOR K IS
C      RETURNED BY GUESS IN THE VARIABLE K0
185  C
C      FRSK = K0
C      ERRMAX = AMAX1(FRSK,ERRMAX)
C
190  C
C      INCREMENT KOUNT. IF 500 (MU, K) PAIRS HAVE
C      BEEN CALCULATED AND STOPK NOT REACHED AN
C      ERROR MESSAGE IS PRINTED, A FIN ERROR IS
195  C      GENERATED, AND THE JOB ABORTED. EITHER RE-
C      DUCE STOPK OR INCREASE THE DIMENSION OF
C      SAVEK(500), SAVEMU(500), TEMPK(500), TEMPMU(500).
C      THEN CHANGE THE TEST ON KOUNT
C
C      KOUNT = KOUNT + 1
200  C      IF (KOUNT .GE. 500) CALL ERRPRN(10)
C      SAVEK(KOUNT) = K1
C      SAVEMU(KOUNT) = MU
C
C      CALCULATE THE LOWER K ESTIMATE FOR THE NEXT
C      MU VALUE
205  C      INCREMENT MU
C
C      K0 = K1 + TDDEL * K1 / MU
C      IF (K0 .GT. STOPK) GO TO 200
210  C      MU = MU + TDDEL
C      96 FORMAT(1X,13,2(=X,F20.5))
C      GO TO 200
C
C      WE ARE FINISHED WITH THIS BRANCH
215  C
C      300 CONTINUE
C      NPTS=KOUNT
C
C      SAVE CURRENT (MU,K) PAIRS TO USE IN ESTIMATING
220  C      K1 ALONG THE NEXT MOVE
C
C      DO 900 I=1,KOUNT
C      TEMPK(I)=SAVEK(I)
225  C      900 TEMPMU(I)=SAVEMU(I)
C      CALL OUTPRN(K,KOUNT)
C
C      PRINT THE MAXIMUM ERROR ESTIMATED FOR K FOR

```

PROGRAM NISPEP

```

C      THIS MODE
230 C      PRINT 98, MODE, FPRK
      98 FORMAT(' ESTIMATED MAXIMUM ERROR IN K FOR MODE ', I4, ' IS ',
1F22.7)
C      BEGIN THE NEXT BRANCH
235 C      MODE = MODE + 1
      IF (MODE .GT. STOPMU) GO TO 400
1000 CONTINUE
      NT = 0
240 C
      MU0 = XMU0(MU0,NV)
      K0 = 0.
      MU = MU0
      KOUNT = 0
245 C      TDEL = XDEL
      LFCUNT = 0
201 CONTINUE
C      FIRST APPROXIMATION OF K FOR THIS BRANCH
C      BEGINS BY FINDING THE K FOR THE LAST BRANCH
250 C
      DO 20 I=1,NPTS
      IF (TEMPMU(I) .GE. MU) GO TO 20
20 CONTINUE
255 C      I = NPTS + 1
      30 SLOPE = TEMPK(I-1) / TEMPMU(I-1)
C
C      CALCULATE THE UPPER ESTIMATE OF K, K1
C
260 C
      K1 = SLOPE * MU
C
C      CALL SUBROUTINE GUESS TO IMPROVE THE ESTIMATE K
C      K1 IS UPPER ESTIMATE, K2 IS LOWER ESTIMATE. THE
265 C      IMPROVED ESTIMATE IS RETURNED IN K1.
C      CALL GUESS(K0,K1,MU)
C
C      CHECK FOR ERROR CODES RETURNED IN NT
270 C
C      NT = 0      A BRANCH WE ANTICIPATED BUT NOT
C                  OCCUR HERE. A RESULT OF OUR ESTI-
C                  MATION PROCEDURE FOR MU.
275 C
C      IF (NT .EQ. 9) GO TO 1000
C
280 C      221 CONTINUE
C
C
C      THE MAXIMUM ESTIMATED ERROR FOR K IS
285 C      RETURNED BY GUESS IN THE VARIABLE K0
C

```

PROGRAM DISPEN

```

C
C      FDSK = K0
C      ERRMAX = AMAX1(FDSK,ERRMAX)
290  C
C
C      INCREMENT KOUNT. IF 500 (MU, K) PAIRS HAVE
C      BEEN CALCULATED AND STOPK NOT REACHED AN
C      ERROR MESSAGE IS PRINTED. A FIN ERROR 52
295  C      GENERATED. AND THE JOB ABORTED. EITHER RE-
C      DUCE STOPK OR INCREASE THE DIMENSION OF
C      SAVEK(500),SAVEMU(500),TEMPK(500),TEMPMU(500).
C      KOUNT = KOUNT + 1
C      IF (KOUNT .GE. 500) CALL FDSKERR(IER)
300  C      SAVEK(KOUNT) = K1
C      SAVEMU(KOUNT) = MU
C
C      CALCULATE THE LOWER K ESTIMATE FOR THE NEXT
C      MU VALUE
305  C      INCREMENT MU
C
C      K0 = K1 + TDELTA * K1 / MU
C      IF (K0 .GT. STOPK) GO TO 300
C      MU = MU + TDELTA
310  C      GO TO 201
C
C
C      400 CONTINUE
C      LMC = SAVEMU(KOUNT)
315  C      ENDDOILE 2
C      REWIND 2
C      CALL PLOTFR(NPTS,1,KMAX)
C
C
C      POSITION THE FILE TO THE BEGINNING OF
C      THE FIRST MODE
320  C
C
C      READ(2,95)R,X0,STOPK,EPK,ND,STOPMU
325  C      95 FORMAT(4E14,7I20,/)
C      PRINT PARAM
C      ISTOP = ND - 1
C      READ(2,94) (N(I), I = 1, ISTOP)
330  C      94 FORMAT(8F10,5)
C      DO 6000 J = 1, ISTOP
C
C      NOW TO CALCULATE OMEGA FOR EACH MODE AND
C      PLOT OMEGA VS K
335  C
C      USE ARRAY SAVEMU TO HOLD THE OMEGA VALUES
C
C      READ(2, 99)NPTS
C      DO 5000 I = 1, NPTS
340  C      READ(2, 100) SAVEK(I), MU
C      SAVEMU(I) = SAVEK(I) / MU
C      99 FORMAT(//,I2)
C      100 FORMAT(2E22,7)

```

PROGRAM DISPFR

```
      101 FORMAT(IX,2E22,7)
      5000 CONTINUE
345      CALL PLOTFR(NPTE.2,KMAX)
      4000 CONTINUE
      CALL PLOTFR(NPTE.3,ERRMAX)
      CALL ENDPI OT
350      C
      C      JOB IS COMPLETE
      C
      STOP
      END
```

FUNCTION XMU0

```

1      FUNCTION XMU0(Y,DY)
      COMMON PSI(500),X(504)
      REAL MU
      MU = Y + DY
5      CALL DIFF(MU,0.,PSIMAX)
      KOUNT = 0
1000  CONTINUE
      TEST = PSI(1)
      KOUNT = KOUNT + 1
      IF(KOUNT.GT. 40)CALL FORPR0(7)
10     MU = MU + DY
      CALL DIFF(MU,0.,PSIMAX)
      IF(TEST * PSI(1).GT. 0.)GO TO 1000
      XMU0 = MU
15     RETURN
      END

```

# SUBROUTINE GUESS

```

1      CHECK GUESS
      SUBROUTINE GUESS(K0,K1,MU)
      COMMON/INDITE/R,ND,AA,EDS,STOPMU,STOPK,STUDA
5      COMMON PSJ(500),N(500),NO,DIFF,AX,NT,ITITLE
      REAL NU,N,MU,K1,K0,K2
      IERR = 2

      C
      C
      C THE MAXIMUM ESTIMATED ERROR FOR K IS
10     RETURNED BY GUESS IN THE VARIABLE K0
      C
      C
      C IF (K0 .EQ. 0.) EPSK = 2.
15     C
      C SOLVE DIFF EQUATION WITH MU, K0
      C IF K0 CLOSE ENOUGH, RETURN WITH K1 = K0
      C
      C
      C
      C
20     C
      C ATTEMPT TO FIND AN UPPER BOUND THAT IS
      C CLOSER TO K0. THIS IS MORE EFFICIENT FOR
      C THOSE CASES WHERE K0 IS A MUCH CLOSER ESTI-
      C MATE THAN K1.
25     C
      C COUNT = 0
      C CALL DIFF(MU, K0, PSIMAX)
      C IF (ABS(PSI(1) / PSIMAX) .GE. EPS) GO TO 10
      K1 = K0
30     C
      C NO ESTIMATE OF THE ERROR IN K POSSIBLE
      C
      C
      C PRINT 98, K0, MU
35     98 FORMAT(' NO ERROR ESTIMATE IN K POSSIBLE HERE', /, ' K0 = ', F22.7)
      C 1 SX: * MU = ', F22.7)
      K0 = EPSK
      RETURN
40     10 CONTINUE
      TEMPMX = ABS(PSI(1) / PSIMAX)
      TEMPK = K0
      TEST = PSI(1)
      STEP1 = (K1 - K0) / 10.
      K1 = K0
45     DO 20 I = 1, 10
      K1 = K1 + STEP1
      CALL DIFF(MU,K1,PSIMAX)
      TERM = ABS(PSI(1) / PSIMAX)
      IF (TERM .GE. EPS) GO TO 20
50     TERM1 = ABS((K1 - TEMPK) / (TERM - TEMPMX)) * EPS
      IF (TERM1 .GT. EPSK) EPSK = TERM1
      K0 = EPSK
      K1 = K1 - TERM1
      RETURN
55     20 CONTINUE
      TEMPK = K1
      TEMPMX = TERM

```



# ROUTINE GUESS

```

        IF (PSI(1) * TEST .LT. 0.) GO TO 201
60      202 CONTINUE
        C
        C
        C      ERROR, NO SIGN CHANGE
        PRINT 99,MU,K0,K1,TEST,PSI(1)
        99 FORMAT(1X,3F20.15)
65      IF (K0 .NE. 0.) GO TO 250
        NT = 9
        RETURN

        C
        C
        C
        C
        C      NOW USE THE REGIM A FAST METHOD
        C
75      201 CONTINUE
        KOUNT = 0
        NCHECO = 0
        NCHEC1 = 0
        200 K2 = K0 + TEST * (K1 - K2) / (TEST - PSI(1))
        KOUNT = KOUNT + 1
        IF (KOUNT .GT. 24) GO TO 240
        SAVE = PSI(1)
        CALL DIFF(MU,K2,PSIMAX)
        TERM = ABS(PSI(1) / PSIMAX)
        IF (TERM .GE. EPS) GO TO 210
        TERM1 = ABS((K2 - TEMPK) / (TERM - TEMPMX)) * EPS
        IF (TERM1 .GT. EPS) EPSK = TERM1
        K0 = EPSK
        K1 = K2 - TERM1
        RETURN
90      210 CONTINUE
        TEMPK = K2
        TEMPMX = TERM
        IF (TEST * PSI(1)) 220,220,220
95      C
        220 CONTINUE
        226 CONTINUE
        K0 = K2
        TEST = PSI(1)
        PSI(1) = SAVE
        GO TO 200
        230 CONTINUE
        236 CONTINUE
        K1 = K2
        GO TO 200
105      240 CONTINUE
        SAVE = PSI(1)
        C
        C
        C      INTERVAL HALVING
110      C
        KOUNT = 0
        285 CONTINUE
        KOUNT = KOUNT + 1
        IF (KOUNT .GT. 34) GO TO 290

```

# ROUTINE GUESS

```

115      TEMPK = K2
      TEMPMX = TERM
      K2 = (K1 + K2)/2.
      CALL DIFF(MU, K2, PSTMAX)
      TERM = ABS(PST(1)/PSTMAX)
120      IF (TERM .LT. EPSIGN TO 700
      TERM1 = ABS(K2-TEMPK)/K2
      IF (TERM1 .LT. 1.E-6) GO TO 300
      IF (TEST * PST(1) .LT. 0.) GO TO 280

125      C      K1 AND K2 ARE ON THE SAME SIDES
      C
      C      K1 = K2
      C      TEST = PST(1)
      C      GO TO 285
130      280 CONTINUE
      C
      C      K1 AND K2 ARE ON OPPOSITE SIDES
      C
      C      K1 = K2
      C      SAVE = PST(1)
      C      GO TO 285
135      290 CONTINUE
      C
      C      ERROR PROCESSING
140      C
      C      NT = 99      INDICATES OVER 50 ITERATIONS
      C                     HAVE OCCURED. BUT NO SATISFACTORY
      C                     ESTIMATE OF K REACHED
145      C
      C      NT = 99
      C      RETURN
      C      250 CONTINUE
150      C      NO SIGN CHANGE HAS OCCURED. EITHER
      C      K1 IS TOO LARGE OR K2 IS TOO SMALL.
      C      THEY LIE ON THE SAME SIDE OF THE
      C      CURVE
155      C      CALL ERRPRO(8)
      C      300 CONTINUE
      C
      C      NORMAL RETURN
160      C
      C      TERM1 = ABS((K2 - TEMPK)/(TERM - TEMPMX)) * EPS
      C      IF (TERM1 .GT. FOUR*EPSK = TERM1
      C      K1 = EPSK
      C      K1 = K2 - TERM1
165      C      RETURN
      C      END

```



```

C
C      OUTPUT
60  C      REAL ARRAY THAT HOLDS THE
C      MODE FUNCTION
C      DIMENSIONED 500
C
C      COMMON/INPUTS/R,ND,X0,EPS,STOPM,STOPX,STOPI
65  C      COMMON PSI(500),N(500),NO,DELTA,INT,ITITLE
C      REAL K,MI,KI,K0,N,MI0,MU1,NO
C      IATFGR,STOPM
C      NAMELIST/INPUT/R,ND,X0,EPS,IFIRST,LAST,K,STOPX
C      PI = ACOS(-1.)
70  C      IFR=9
C
C      READ THE IDENTIFYING PARAMETERS
C      FROM TAPES
75  C
C      READ (5,9A) R,X0,STOPK,EPS,ND,STOPM
C
C      READ INPUT
80  C      K,STOPX,IFIRST,LAST
C      READ INPUT
C
C      PRINT NAMELIST/INPUT, FOR VERIFI-
85  C      CATION: THEN PRINT N(X)
C      PRINT INPUT
90  C
C      IF(K.GT. STOPK) CALL ERORNO(TEW,1)
C      IF(LAST.GT. STOPM) CALL ERORNO(IFR,2)
C
C      CALL INITIAL TO READ THE VALUES
95  C      OF N(X) OFF TAPE 5
C      GET N(X) DATA AND CALCULATE DELTA
C
C      CALL INITIAL(SUM1)
100  C      PRINT 101,(N(I),I=1,ND)
C      PRINT 99
C
C      ISTOP = ND - 1
105  C
C      DELTAMU = PI / SUM1
C      IF(IFIRST.EQ. 1) GO TO 105
C
C      ADVANCE POINTER TO THE
110  C      FIRST MODE OF INTEREST. IFIRST
C
C      ISTOP = IFIRST - 1
C      DO 500 I = 1, ISTOP

```

PROGRAM MODE

```

115      READ(5,99)NPTS
          DO 500 J = 1, NPTS
              READ(5,100)DUMMY,DUMMY
          500 CONTINUE
120      505 CONTINUE
          CALL PLOTS(100,0)
          DO 510 I = IFIRST, LAST
              C
              C
              C      FOR EACH OF THE MODES
125      C
              READ(5,99)NPTS
              K0 = 0
              MU0 = (1 + .5) * DELTAMU
              DO 520 J = 1, NPTS
130      C
              C      READ EACH (K, OMEGA) PAIR TO FIND K INTERVAL
              C
              READ(5,100)K1,MU1
              IF(K1.GT. K)GO TO 530
135      K0 = K1
              MU0 = MU1
              520 CONTINUE
              530 CONTINUE
140      C
              C      DO LINEAR INTERPOLATION
              C
              SLOPE = (K1 - K0) / (MU1 - MU0)
              YINT = K1 - SLOPE * MU1
              MU = (K - YINT) / SLOPE
145      PRINT 99
              PRINT 101 ,MU,K
              C
              C      SOLVE DIFFERENTIAL EQUATION
              C
150      CALL DIFF,MU, K, PSIMAX,
              CALL INTNP(K, MU, SUM3)
              AMAXN = PSIMAX / SORT(SUM3)
              U = S_OPX / DELTAX + 1
155      C
              C      ERROR CONNECTION
              C      CHECK THAT NUM NOT GREATER THAN THE DIMENSION OF N
              C
              IF(NUM.GT. 500,CALL ERORNO,IER)
160      C
              C      FILL IN THE REST OF PSI
              C
              NT = NUM - ND
              TINDX = K * R
              ARG = MU * R * ND
165      DO 560 L = 1, NT
              CALL JUESS(TINDX, 1, ARG * EXP(-(L + 1) * DELTAX / B1),
              1 PSI(ND + L))
              560 CONTINUE
170      C
              C      NORMALIZE
              C

```

PROGRAM MUDF

```

      DO 570 L = 1, NUM
      PSI(L) = PSI(L) / SQRT(SUM3)
175      570 CONTINUE
      C
      C      DO PLOTTING AND OUTPUTTING HERE
      C
      PRINT 98, I
180      PRINT 101, (PSI(I), I = 1, NUM)
      CALL PLOTMOD(NUM, I, K, K / MU, AMAXN)
      ISTART = J + 1
      C
      C      ADVANCE POINTER TO NEXT MUDF
185      C
      DO 580 J = ISTART, NPTS
      READ(5, 100) DUMMY, DUMMY
      580 CONTINUE
      510 CONTINUE
190      CALL ENDPLOT
      STOP
      101 FORMAT(1X, 4F22.7)
      100 FORMAT(2E22.7)
      99 FORMAT(//, 15)
195      98 FORMAT(1H1, * MUDF NUMBER *, I3)
      96 FORMAT(4E15.7, 2I5//)
      END

```

SUBROUTINE DIFF

```

1      *DECK DIFF
      SUBROUTINE DIFF (M1,K,PSIMAX)
      COMMON/INPUTS/R,ND,XA,ESS,STOPMU,STOPK,STUDB
5      COMMON PSI(500),N(500),ND,DELTAX,NT,ITITLE
      REAL NU,N,M1,K,M0

      C
      C
      C      THIS IS THE NUMEROV - MANNING - MILLMAN METHOD
      C      FOR SOLVING SECOND ORDER LINEAR DIFFERENTIAL
10     C      EQUATIONS
      C
      F(X)=K**2 - MU**2 + Y**2
      DPSI(X,Y) = F(X)*Y
      M0=R*NU
      ISTOP = ND

      C
      C      DEFINE FIRST TWO VALUES OF PSI
      C
      TEMP1=K*B
      TEMP2=MU*M0
20     CALL JHESC (TEMP1,TEMP2*EXP(-DELTAX / B),PSI(1))
      CALL JHESC (TEMP1,TEMP2,PSI(2))
      TERM=DELTAX**2/12.
      PSIMAX = ABS(PSI(2))

25     C
      C      SOLVE THE EQUATION BACKWARDS
      C
      DO 100 I=3,ISTOP
      VALM=2.*PSI(I-1)-PSI(I-2)
30     XNUM=XNUM+DPSI(M*(ND-I+1),PSI(I-2))*TERM
      XNUM=XNUM+DPSI(M*(ND-I+1),PSI(I-1))*TERM+1.
      DENOM=1.-TERM*(N(ND-I+2))
      PSI(I)=XNUM/DENOM
      TFR=LEGVAR(PSI(I))
      IF(IERR.NE.0) GO TO 900
35     100 PSIIMAX = AMAX1(ABS(PSI(I)),PSIMAX)
      JSTOP = ISTOP / 2

      C
      C      REORDER PSI
40     C
      DO 200 I = 1, JSTOP
      INDEX=ISTOP+1-I
      TEMP=PSI(I)
      PSI(I)=PSI(INDEX)
45     200 PSI(INDEX)=TEMP
      RETURN
900 CONTINUE
      IF(IERR.EQ.1) TFR=0
      CALL ERRPON(IERR + 3)
50     END

```

# SUBROUTINE INTNP

```

1      *DECK INTNP
      SUBROUTINE INTNP(K,MU,SUM3)
      COMMON/INPUTS/H,NQ,XA,EOS,STOPMU,STOPK,STOPI
      COMMON PSI(500),N(500),NO,DEFI,TAX,NT,ITITLE
5      COMMON /FINC/ ARG
      REAL NU,N,MU,K
      EXTERNAL FUNCT2, FUNCT4
      ARG = K
      SUM3 = .5*((N(1)*PSI(1))**2 + (N(NQ)*PSI(NQ))**2)
10     TERM=MU*H*NO
      ISTOP=NO-1
      DO 100 I=2,ISTOP
100    SUM3=SUM3+(N(I)*PSI(I))**2
      SUM3 = SUM3 * DEFI TAX
15     TEST = (2. * K * B)**2
      TEST = ABS((TEST - 1.) * (TEST - 9.))
      TEST = TEST / 128. * 1.E3
      TEST = SQRT(TEST)
      UPPER = AMIN1(TEST, TERM)
20     Z= GAUSS(4, 0., UPPER, FUNCT2)
      IF (TERM .GT. TEST) Z = Z + GAUSS(4, TEST, TERM, FUNCT4)
      Z = Z / MU**2
      SUM3=SUM3+Z/A
      RETURN
25     END

```



FUNCTION FUNCT2

```
1      FUNCTION FUNCT2(X)
      COMMON/INPUTS/R,ND,XA,EDS,STOPMU,STOPK, STUPX
      COMMON PSI(SA0),N(SA0),NG,DELTAX,NT,ITITLE
      COMMON /FUNC/K
5      REAL NU,N,K
      CALL JBESS(K*8,1,X,BESS)
      FUNCT2=BESS**2*X
      RETURN
      END
```

FUNCTION FUNCT4

```

1      FUNCTION FUNCT4(X)
        COMMON/INPUTS/A,N0,X0,EPS,STOPM1,STOPK,STUAX
        COMMON PST(500),N(500),NO,NELTAX,NT,I7ITLF
        COMMON /FUNCT/ K
5         REAL NU,N,K

          C
          C
          C      ASYMPTUTIC APPROXIMATION FOR J(K*B, X), B=20A
          C
10        PJ = ACOS(-I.)
            TERM1 = 2. /PI
            TERM2 = K*B
            ARG = X - (.5 * TERM2 + .25) * PI
15           TERM3 = (.4 * TERM2 ** 2 - I.) / (A. * X)
            FUNCT4 = TERM1 * (COS(ARG) - TERM3 * SIN(ARG))**2
            RETURN
          END

```

# SUBROUTINE INITIAL

```

1          SUBROUTINE INITIAL (SUMI)
            COMMON/INPUTS/R,ND,X0,EPS,STOPMU,STOPK,STOPI
            COMMON PSI(500),N(500),N0,DELTAX,NT,ITITLE
            REAL NU,N

5          C
            C
            C          CALCULATE DELTAX FROM X0 AND ND
            C
10         C          DELTAX = X0 / (ND - 2)
            C
            C          READ NUMERICAL VALUES
            C
15         C          ISTOP = ND - 1.
            C          READ(5,450) ITITLE
            C          450 FORMAT(A10)
            C          READ(5,400) (N(I),I = 1,ISTOP)
            C
            C          CALCULATE X0,H VALUE OF N
20         C
            C          N0 = N(ND-1)
            C          N(ND) = N0 * EXP(-DELTAX/H)
            C
            C          CALCULATE THE INTEGRAL OF N
25         C
            C          SUMI = 0.5*(N(1)+N(ND))
            C          ISTOP = ND - 1
            C          DO 300 I = 2,ISTOP
            C          300 SUMI = SUMI + N(I)
30         C          SUMI = SUMI * DELTAX
            C          SUMI = B * N0 + SUMI
            C          RETURN
            C
            C          ERROR PROCESSING
35         C
            C          700 CALL EHRPRO(1)
            C          RETURN
            C          400 FORMAT(8F10.5)
            C          END

```

# SUBROUTINE OUTPUTK

```

1      CHECK OUTPUT
      SUBROUTINE OUTPUTK (KOUNT)
      COMMON /INPUTS/ R,ND,XA,EOS,STOPMU,STOPK,STOPX
      COMMON PSI(500),N(500),MU,DELTA,XINT,ITITLE
      INTEGER STOPMU
      REAL MU, N
      COMMON /OUT/ X(500), Y(500)
      IF (KOUNT .NE. 1) GO TO 50

10     C
      C
      C      WRITE IDENTIFYING PARAMETERS TO TAPE 2
      C      FOLLOWED BY THE VALUES OF N(X)
      C
15     C
      C      WRITE(2,9A) R,XA,STOPK,EOS,ND,STOPMU
      C      ISTOP = ND - 1
      C      WRITE(2,9A) (N(I),I=1,ISTOP)
      C      RETURN
      C      50 CONTINUE

20     C
      C
      C      PRINT NUMBER OF PAIRS AND LIST
      C      THE PAIRS TO OUTPUT
      C
25     C
      C      WRITE THE NUMBER OF PAIRS AND
      C      THE PAIRS TO TAPE 2
      C
      C
      C      PRINT 98,KOUNT
      C      WRITE(2,9A) KOUNT
      C      DO 10 J=1,KOUNT
      C      WRITE(2,100) X(J),Y(J)
30     10 PRINT 101,X(J),Y(J)
      C
      C      RETURN
      C      98 FORMAT(1H1,15)
35     99 FORMAT(4E15.7,2I4//)
      C      99 FORMAT(8F10.4)
      C      101 FORMAT(1X,2E22.7)
40     99 FORMAT(//,15)
      C      100 FORMAT(2E22.7)
      C
      END

```

# SUBROUTINE ERRPRC

```

1          SUBROUTINE ERRPRC (N)
C
C          THIS ERROR PROCESSING SUBROUTINE PRESUPPOSES
C          AN I/O TYPE ENVIRONMENT WITH CDC 6400 EQUIP-
5          MENT, NOS/REI OPERATING SYSTEM
C
C          THE EXTERNAL REFERENCE ABRTJOB IS A ROUTINE
C          WRITTEN IN COMPASS TO GENERATE ERROR MESSAGES,
C          INITIATE TRACE BACK, AND ABORT THE
10         JOB WITH OUT A DUMP
C
C          GO TO (700,800,900,902,1001,1002,1003,1004,1005,1006,1007,N
1005      CALL ABRTJOB(400 L MORE THAN 400 PAIRS WERE NEEDED FOR THIS BRANCH)
1006      CALL ABRTJOB(600 L THE MAXIMUM K VALUE ON TAPES IS LESS THAN THE K
15         1007      CALL ABRTJOB(300 L THERE ARE NOT ENOUGH MODES ON TAPE)
C          1007      CALL ABRTJOB(300 L THERE ARE NOT ENOUGH MODES ON TAPE)
C          700      CALL ABRTJOB(200 END-OF-FILE, UNIT 5)
C          800      CALL ABRTJOB(160 COUNT TOO LARGE )
C          900      CALL ABRTJOB(200 INDEFINITE OPERAND 0 / 0 )
20         902      CALL ABRTJOB(100 DIVISION BY ZERO)
1001      CALL ABRTJOB(300 CANNOT FIND MU0 FOR THIS MODE)
1002      CALL ABRTJOB(160 TOO MANY POINTS)
1003      CONTINUE
1004      CALL ABRTJOB(330 K0 AND K1 ON SAME SIDE OF CURVE )
25         END

```

# SUBROUTINE PLOTMOD

```

1      SUBROUTINE PLOTMOD(NPTS,MONE,XK,XOM,STEP)
      COMMON/INPUTS/R,NO,XA,EPG,STOPMU,STOPK,STUPA
      COMMON PST(500),N(500),NO,DELTA,NT
      DIMENSION DEL(4),XX(11),YY(11),XPLOT(500),YPLOT(500)
5      EQUIVALENCE(PST,YPLOT)
      DATA DEL/5.,0.,0.,1./
      DEL(4) = STEP*2.
      CALL PSSCALE(DEL(4))
      DEL(2) = STOPK / 10.
10     DO 100 I=1,11
      XX(I) = (I - 1) * DEL(2)
      YY(I) = (I - 6) * DEL(4)
100    CONTINUE
      DO 200 I=1, NPTS
15     XPLOT(I) = (I - 1) * DELTA
200    CONTINUE
      CALL DAXIS(0.,0.,10HPSI SEP/SUNT(MFTER),-14.4,5.90.,YY,1.,4HF6,1,
1      6)
      CALL PLOT(0.,5.,-1)
20     CALL SYMBOL(.5,4.5,.1,PHK=,0.,2)
      CALL NUMBER(.8,4.5,.1,XK,0.,4HF4,2,4)
      CALL SYMBOL(.5,4.,.1,OMEGA=,0.,4)
      CALL NUMBER(1.2,4.,.1,XOM,0.,4HF7,4,7)
      CALL DAXIS(0.,0.,15HDEPTH IN METERS,15,10.,0.,XX,1.,4HF7,2
25     ,7)
1      CALL SYMBOL(2.,4.,.2,11HMODE NUMBER,0.,11)
      CALL NUMBER(4.4,5.,.5,MONE,0.,2H13,3)
      CALL LINE(XPLOT,YPLOT,NPTS,1,0,0,DEL)
      CALL PLOT(12.,4.,-1)
30     RETURN
      END

```

# SUBROUTINE PLOTFR

```

1      *CHECK PLOT
      SUBROUTINE PLOTFR(NPTS,M,KMAX)
      COMMON/OUT/XPLOT(500),YPLOT(500)
5      COMMON/INPUTS/R,ND,X0,EPS,STOPMU,STOPK,STUDX
      PST(500),N(400),N0,DELTAX,NT,ITITLEP
      DIMENSION DEL(4),XX(1),YY(1)
      REAL KMAX
10     GO TO(10,20,30)M
      CONTINUE
15     DEL(1) = 0
      DEL(2) = STOPK / 100
      DEL(3) = 0
      DEL(4) = KMAX
      CALL PSCALE(DEL(4))
      DO 100 I = 1, 11
15     XX(I) = (I-1) * DEL(2)
      YY(I) = (I-1) * DEL(4)
20     CALL PLOTFR(100,0)
      CALL DAXIS(0,0,100K (GAUSSIANS / METER),10,10,0,XX,1,4HF6.4,6)
      CALL SYMBOL(2,0,0,21,74HINTERNAL WAVE DISPERSION RELATIONS,0,0
      * 34)
      CALL SYMBOL(4,0,5,51,1TITILE,0,10)
      CALL DAXIS(0,0,5HOMEGA,0,10,90,YY,1,4HF6.4,6)
25     RETURN
20     CALL LINE(XPLOT,YPLOT,NPTS,1,0,0,DEL)
      CALL PLOT(0,0,0,1)
      RETURN
30     CONTINUE
35     CALL SYMBOL(4,5,5,51,21HMAXIMUM ERROR IN K IS,0,21)
      F=1.
      CALL WHERE(XOLD,YOLD,F)
      CALL NUMBER(XOLD,YOLD,51,KMAX,0,0,HE10,3,10)
      RETURN
99     FORMAT(1X,F20.10)
      END

```

SUBROUTINE DSCALE

```

1          SUBROUTINE DSCALE(SCALE)
          TERM=1.
          IF(SCALE .GE. 1.) GO TO 2
5          J=SCALE*TERM
          IF(J.GT.0) GO TO 10
          TERM = TERM * 10.
          GO TO 1
          2 J=SCALE/TERM
          IF( J .LE. 10) GO TO 20
10         TERM=TERM*10.
          GO TO 2
          10 SCALE=(J+.5)/(10.*TERM)
          RETURN
          20 SCALE=(J+.5)*TERM/10.
15         RETURN
          END

```



**DATE**  
**FILME**